



### SOFIP:

# A Short Orbital Flux Integration Program

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#### ABSTRACT

A computer code has been developed to evaluate the space radiation environment encountered by geocentric satellites. The Short Orbital Flux Integration Program (SOFIP) is a compact routine of modular composition, designed mostly with structured programming techniques in order to provide not only maximum efficiency but also core and time economy and ease of use. program in its simplest form, that is, stripped of all modules, produces for a given input trajectory a composite integral orbit spectrum of either protons or electrons. Additional features such as running printout, exposure index, peaks per orbit, percent time in electron trapping zones, differential spectrum, solar proton fluences, and punched output are available separately or in any combination with the inclusion of the corresponding (optional) modules. The code is described in detail, and the function and usage of the various modules are explained. A program listing and sample outputs are attached.

#### CONTENTS

<u>Pa</u>	ge
INTRODUCTION	1
THE CURRENT ENVIRONMENT MODELS	2
METHOD	3
Integral Flux	3
Difference Flux	3
Differential Flux	3
APPLICATION AND USE	4
BLOCK O: Initialization	4
BLOCK 1: Initialization	5
BLOCK 2: Input	6
BLOCK 3: Calculations	7
Running Printout Module	7
Orbit L-Zone Breakdown Module	7 '
Exposure Index Module	8
Peaks-per-Orbit Module	8
Geomagnetic Shielding Module	8
BLOCK 4: Looping	9
BLOCK 5: Output Preparation	9
Percent Time Module	9
Differential Spectrum Module	9
Solar Proton Module	9
	0
Output-Tables Module 1	0
Output-Tables Module 2	1

#### CONTENTS CONT.

		raye
BL	OCK 6: Program Termination	11
ACKNOWL	EDGEMENTS	12
REFEREN	CES	13
	LIST OF TABLES	
<u>Table</u>		Page
1	Running Times of SOFIP for 720 Input Positions	14
2	Core Requirements for SOFIP	15
3	Input Parameters: Description and Format	16
4	Punched Output: Description and Format	17
		`
	LIST OF FIGURES	
Figure		<u>Page</u>
1	Modular Structure and Arrangement of SOFIP	18
2	Flow Diagram for SOFIP	19
,		
,		
ATTACHM	MENTS: PROGRAM LISTINGS AND SAMPLE OUTPUTS	

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#### INTRODUCTION

The need to predict reliably satellite exposure to trapped particle radiation was realized soon after the discovery of the terrestrial charged particle radiation belts, which coincided with the advent of spaceflight. A crude "Orbital Flux Integration" (OFI) code was developed at Goddard Space Flight Center as early as 1961. Over the years, a large, sophisticated, and complex OFI system evolved from these early beginnings (UNIFLUX¹), a system that processed and analyzed the data into several different tabular and graphical presentations.

However, with the appearance of economical minicomputers and the corresponding emphasis on small software systems, attributes like "compact", "short", "fast", and "versatile" became very important.

In this paper a Short Orbital Flux Integration Program (SOFIP) is being presented which, excluding the plotting capability, affords all the options, choices, and variations of UNIFLUX, but with substantially reduced core requirements and running times.

Two basic guidelines influenced the creation of SOFIP: structured programming and modularized organization. These were followed to the greatest degree possible or desirable.

A detailed description of the routine is given in subsequent sections, including an analysis of the method employed in the determination of integral, difference, and differential fluxes.

A review of the program organization is given in Figure 1 which depicts the structure of the fully implemented (complete) code. Logic flow and decision branching is shown in Figure 2.

The arguments of its input and output vectors (variables and parameters) are presented and described in the appropriate sections. Code listing and sample outputs are attached.

SOFIP is written in standard FORTRAN-IV computer language. Card decks are available from the National Space Science Data Center in the 029 model IBM keypunch format (EBCDIC). The cards are labelled in columns 73-80 as SOFIPxxx, where the last three columns (xxx) contain the sequential numbering, which is incremented by one.

A comparison of the time required to compile, linkage edit, and execute SOFIP is given in Table 1. The data relate to full length and stripped versions of the code, and were obtained for both electron and proton runs, by processing 720 positions in each case.

The approximate amount of storage required by SOFIP is given in Table 2, for the various parts of the program, including also the environment models, in object form.

All results were obtained on GSFC's IBM 360/91 and, unless otherwise stated, using the FORTRAN IV G compiler.

#### THE CURRENT ENVIRONMENT MODELS

SOFIP is designed to use Vette's standardized models of the terrestrial trapped particle environment, as distributed by the National Space Science Data Center, Greenbelt, Maryland. New models are periodically being issued to replace older versions whenever additional data or information become available that permit a significant improvement in the environment description, or that indicate a change sufficiently important to warrant such an action. All models, both for protons and electrons, represent a static environment at a given fixed epoch. However, it was possible to infer from the data used in their construction a change in average quiet-time flux levels as a function of solar cycle. To date, a continuous temporal description of this cycle dependence has not been attempted. Instead, separate models were developed for solar minimum and solar maximum conditions for either species of particles.

Current at the time of this writing are the following models:

		Solar Max	<u>Solar Min</u>
Protons:		AP8-MAX (1970) <sup>2</sup>	AP8-MIN (1964) <sup>2</sup>
Electrons:	Inner Zone:	AE6 (1980) <sup>3</sup>	AE5 (1975) <sup>4</sup>
	Outer Zone:	AEI7-HI	(1980) <sup>5</sup> (1980) <sup>5</sup>

where the numbers in parentheses indicate the specific fixed epoch (year) for which they describe the average environment.

In regards to the outer zone electron models AEI7-HI and AEI7-LO it should be noted that:

- (a) the version labelled "HI" favors Vampola's fits to the OV1-19 data, while the version labelled "LO" is representative of all the other outer zone data sets presently available at NSSDC.
- (b) these models do not reflect solar cycle conditions and should be used indiscriminately for both min and max phases.
- (c) they are interim models which recently replaced the solar min and max versions of the older AE4.

It should also be noted that the inner zone (solar max) AE6 does not contain any "Starfish" residuals because data now indicate that these electrons are no longer present. 6

**METHOD** 

#### Integral Flux

The composite orbit spectrum for integral energies gives the total vehicle encountered fluxes, averaged into intensities per second, for 30 discrete energy levels:

 $S(>E_i) = c\Delta t \sum_{m=0}^{T} (>E_i)$ 

c=24/T\*86400

where the summation is performed for the entire simulated mission duration  $T_s$  in hours, and includes all fluxes with energies greater than  $E_i$ .  $\Delta t$  is the integration step-size in seconds,  $J_m$  is the instantaneous integral flux obtained from the model for the  $i^{th}$  energy level, and c is an averaging factor. Note that  $\Delta t$  must have values equivalent to integer minutes (See also note on page 7).

#### <u>Difference Flux</u>

The difference flux is calculated from the integral flux  $S(>E_i)$  for the 30 programmed energy levels:

$$D(\Delta E_i) = S(>E_i) - S(>E_{i+1})$$
 for i=1, 29  
 $D(\Delta E_{30}) = S(>E_{30})$ 

where D is the difference flux in units of particles per square centimeter per second per energy interval. It is important to remember that E is not constant over either the proton or the electron spectra.

#### Differential Flux

Differential fluxes are only calculated when there exist 10 or more non-zero elements in the integral spectrum. That is, fluxes must be defined for at least ten descrete energy levels. In that case, the differential fluxes are obtained from the composite orbit spectrum by analytic differentiation, using the averaged instantaneous values of the total vehicle encountered fluxes at the selected energies:

$$j(=E_1) = \frac{2S(>E_1)}{2E}$$
 for i=1,30

where j is the differential flux and E and S are the same as above. The results in the program output table represent the derivative of a cubic spline fitting procedure. If there are less than 10 non-zero elements available, the program bypasses these calculations.

#### APPLICATION AND USE

SOFIP contains two types of program sections: blocks, which are the essential parts of the program and must remain unaltered, and modules, which provide additional features and may be removed. For each block and module, the following points are discussed:

- 1. Function (including output produced, if any),
- 2. User input or user action necessary, and
- 3. Any restrictions, limitations, or other special considerations.

There are 11 modules in SOFIP, some of which are paired into packages which fulfill a single purpose. These packages and the output they produce are:

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#### Output

ORBIT L-ZONE BREAKDOWN MODULE PERCENT TIME MODULE

Percent Time Table

PEAKS PER ORBIT MODULE OUTPUT TABLES MODULE 2

Peaks per Orbit Table

GEOMAGNETIC SHIELDING MODULE SOLAR PROTON MODULE

Solar Proton Table

To obtain the desired results from one of these module packages, both modules in the particular package must be included in the run. If one module is included but the other is not, no data will be outputted from the calculation which those modules perform. However, such misuse of the module packages will neither cause the run to abend, nor affect the output of any other portion of the program.

#### BLOCK O: Initialization

BLOCK O performs the general initialization and preparation of the program. It contains all "type" declarations (REAL, INTEGER), and all dimension, equivalence, and format statements.

The user has only to be concerned with one aspect of this initialization: the selection of the environment model(s) to be used. Lines 39-44 of SOFIP contain COMMON statements for all of the current environment models, both proton and electron:

```
C COMMON /AP8MAC/DESCR(8), LIST(1) SOFIPO39
C COMMON /AE6MAX/DESCR(8), LIST(1) SOFIPO40
C COMMON /AE17HI/DESCR7(8), LIST7(1) SOFIPO41
C COMMON /AE17LO/DESCR7(8), LIST7(1) SOFIPO42
C COMMON /AE5MIN/DESCR(8), LIST(1) SOFIPO43
C COMMON /AP8MIC/DESCR(8), LIST(1) SOFIPO44
```

For a brief discussion of the models, see the section "The Current Environment Models".

To select a particular environment model:

- 1. Uncomment the COMMON statement which relates to the desired model, that is, remove the "C' from column one,
- 2. Make sure all other COMMON statements are commented out,
- Include in the deck to be submitted, the BLOCK DATA subroutine for the appropriate model.

Note that protons require only one model per run, while electrons require two, one for the inner zone and one for the outer zone. The two electron models are needed regardless of whether the trajectory to be processed visits only one of the two electron zones.

Because SOFIP performs calculations for only one particle species in a given run, the model(s) for only one species is needed. In other words, any one run will use either one proton model (AP8MAX or AP8MIN) or one inner zone electron model (AE6MAX or AE5MIN) and one outer zone electron model (AE17HI or AE17LO). The program cannot and does not check for invalid combinations of models, nor for BLOCK DATA subroutines and uncommented COMMONs statements incorrectly matched. These user errors will produce compilation, linkage, or execution errors.

Note also that there is no provision for changing models during execution. Therefore, in a multiple-orbit run, all trajectories are processed for the same species and models(s).

When SOFIP is run for electrons, a diagnostic message may be produced during compilation warning that the variable "DESCR7" in line 51 of SOFIP has already been dimensioned. Do not change this dimensioning; it is necessary when the run is for protons. The warning may be ignored.

#### BLOCK 1: Initialization

BLOCK 1 performs the initialization of quantities which must be reinitialized after each orbit of a multiple-orbit run. In this block, the input variables are read and subsequently written out. Table 3 gives the input format and

a brief description of each parameter, two of which require some additional comments:

NRGYLV is the threshold-energy selector. Its value is an index into the ENERGY array. The desired value of NRGYLV is most easily obtained by looking at the Composite Orbit Spectrum from a SOFIP run for the correct particle species, and counting down to the desired energy level. The usual values are: electrons, NRGYLV=5 (0.5 MeV); protons, NRGYLV=4 (5.0 MeV).

CUTOFF determines the orbit time at which processing is to be terminated. If the end of the orbit tape is reached before orbit time reaches CUTOFF, the program will proceed as if CUTOFF had been equal to the time of the last point read. This will not cause any errors in the program.

#### BLOCK 2: Input

In BLOCK 2, the trajectory ephemeris tape is read. The program can read a tape written in either of two modes, BCD or binary. To read a BCD (EBCDIC, or formatted) tape:

- 1. The tape must have been written with format 6E18.8.
- 2. Comment out lines 133-134, 138-139, and 144.
- 3. Uncomment lines 132, 137, and 143.

To read a binary (unformatted) tape:

- 1. The first input variable, PSNTIM (see below) must have been written in single precision; the other five elements must have been written in double precision.
- 2. Comment out lines 132, 137, and 143.
- 3. Uncomment lines 133-134, 138-139, and 144.

For either input mode, each record of the tape must contain the following six variables in the order specified:

PSNTIM	T	Orbit time in decimal hours (must start at 0.0)
PSNLON	ф	East longitude in decimal degrees
PSNLAT	λ	North latitude in decimal degrees
PSNALT	h	Geodetic altitude in kilometers above sea level
PSNB	В	Geomagnetic field magnitude in gauss
PSNL	L	McIlwain's magnetic shell parameter in earth radii

The input parameter ISKIP controls the number of records ignored each time a new point is called for by the program; only each ISKIPth point on the input tape is actually used in performing calculations.

The positional coordinates of longitude, latitude, and altitude are not used in the flux calculations; these calculations are performed with the magnetic parameters B and L only. Therefore, it is of no significance whether latitude relates to a geocentric or a geodetic reference frame (longitude is invariant in the two systems). The altitude, however, is used to determine the position of physical perigee in the case of eccentric trajectories.

NOTE: Do not use trajectories with stepsizes of less than one minute; they will cause the program to abend. Also, the stepsize must be constant for any one orbit, because the time integration assumes that the increment is not a function of orbit position <u>i</u>:

$$\sum_{i} Flux_{i} \Delta t = \Delta t \sum_{i} Flux_{i}$$

#### **BLOCK 3:** Calculations

In BLOCK 3 some preparatory calculations are performed and the fluxes for the current position are obtained. No user action is necessary.

#### Running Printout Module

The "Running Printout Module" prints orbit and flux data for each position i used in the calculations when the input parameter KPRINT is equal to 1. If the input parameter KPRINT is not equal to 1, only each KPRINTth point is printed. The printed quantities are:

Orbit time	Τį	decimal hours
Latitude	λi	decimal degrees
Longi tude	φi	decimal degrees
Altitude	hi	kilometers
Field magnitude	Βį	gauss
Magnetic shell parameter	Li	earth radii
Instantaneous flux	Fi	at the position i (#/cm²· sec)
Time integrated flux	F₁∆t	integrated over the interval from i to i+1
Orbital flux accumulation	J≐ΣFj∆t	sum of all fluxes encountered to this point
	1	

The first six quantities are the same as those read from the ephemeris tape. For the first position of the orbit, only the positional data are printed.

If running printout is not desired, delete this module.

#### Orbit L-Zone Breakdown Module

The "Orbit L-Zone Breakdown Module" determines the amount of time spent by the trajectory in each of the four zones into which magnetic space can be divided on the basis of electron trapping:

1. Inner zone: outside trapping region  $(1.0 \le L < 1.1)$ 

- 2. Inner zone: inside trapping region  $(1.1 \le L \le 2.8)$
- 3. Outer zone (2.8<L<11.0)
- 4. External (no trapping) (L>11.0)

These data will be used for further calculations in the "Percent Time Module".

Note that the "Orbit L-Zone Breakdown Module" <u>must</u> be used in conjunction with the "Percent Time Module". If the percent time information is not desired, delete both modules.

#### Exposure Index Module

The "Exposure Index Module" describes, for the selected processing energy, the radiation exposure in terms of nine intensity ranges, rising from "zero flux" through  $10^{9}-10^{1}$ ,  $10^{1}-10^{2}$ , etc., to "more than  $10^{7}$  particles per square centimeter per second" in increments of one order of magnitude. The overall exposure of the trajectory to each intensity range (in decimal hours) and the total number of particles encountered while so exposed are recorded.

If the exposure index table is not desired, delete this module.

The exposure index is calculated for particles with  $E \ge ENERGY(NRGYLV, species)$  where NRGYLV is the threshold energy selector variable (see section "BLOCK 2" for further discussion of NRGYLV).

#### Peaks-Per-Orbit Module

The "Peaks-per-Orbit Module" determines:

- the instantaneous peak flux per period, in number of particles/cm<sup>2</sup>sec with energies greater than or equal to the threshold energy selected by NRGYLV,
- 2. the time (in hours) and position (in  $h-\phi-\lambda$  and B-L coordinates) at which the peak flux is encountered, and
- the total number of particles accumulated per period.

The "Peaks-per-Orbit Module" <u>must</u> be used in conjunction with the "Output Tables Module 2". If the peak data is not desired, delete both modules.

#### Geomagnetic Shielding Module

This module determines the amount of time the vehicle spends in regions of space where L > 5, for later calculations in the "Solar Proton Module".

The "Geomagnetic Shielding Module", must be used in conjunction with the "Solar Proton Module". If Solar Proton data is not desired, delete both modules.

#### BLOCK 4: Looping

BLOCK 4 concludes the trajectory ephemeris read-loop. All blocks and modules between Block 2 (trajectory input) and Block 4 are executed for each inputted point of the trajectory. No user action is required.

#### BLOCK 5: Output Preparation

In BLOCK 5, the calculations for the composite orbit spectrum are performed. No user action is required.

#### Percent Time Module

The "Percent Time Module" takes the information stored in the "Orbit L-Zone Breakdown Module", i.e., the number of times the vehicle visits each of the four zones defined in that module, and calculates the percent of total orbit time spent in each; this data is then printed.

If the percent time table is not desired, delete both this module and the "Orbit L-Zone Breakdown Module".

#### Differential Spectrum Module

The "Differential Spectrum Module" calls subroutine DSPCTR, which calculates the differential spectrum from the total integral fluxes obtained from the environment models.

If the differential spectrum is desired, include subroutine DSPCTR and this module. If the differential spectrum is not desired, delete this module.

#### Solar Proton Module

This module calculates the exposure factor (i.e., the fraction of the orbit during which the vehicle is not geomagnetically shielded, but is exposed to the interplanetary intensities of energetic solar protons) from the value stored in the "Geomagnetic Shielding Module". It then calls the subroutine SOLPRO $^7$ , which calculates probabilistic solar fluences at preselected energy levels as a function of mission duration  $\tau$  and confidence level Q.

There are two elements in the solar proton module which the user may wish to alter to meet his specific needs:

1. Mission duration  $\tau$ : (REAL\*4, variable name in code: T)

 $\tau$  determines the time interval, in non-fractional months, for which the solar proton calculations are to be performed. The code

is preprogrammed for one year mission duration ( $\tau$ =12). If a different length of time is desired, edit card 276 accordingly. The permissible range of  $\tau$  values is from 1 to 72 months.

2. Confidence level Q: (INTEGER\*4; variable name in code: IQ)

Q denotes the level of confidence, in percent, which the user wishes to assign to the results; namely, that for the specified mission duration the calculated fluences are the smallest values that will not be exceeded by actually encountered intensities. The preprogrammed confidence level is 90%. If a different value of Q is desired, edit card 278 accordingly. Permissible values of the variable IQ are integers between 80 and 99, inclusive.

If the solar proton information is desired:

- 1. include this module and the "Geomagnetic Shielding Module", and
- 2. include subroutine SOLPRO in the deck to be submitted.

Otherwise delete the "Solar Proton" and "Geomagnetic Shielding Modules".

#### Output-Punch Module

This module produces a card deck containing some of the calculated results. Each card, with exception of the header cards, contains a label in columns 73-78 and a sequence number in columns 79-80. The label indicates the particle species and whether the card contains energies, integral fluxes, or differential fluxes. The sequence number will reflect the card's position in the particular section of the deck to which it belongs, e.g., integral fluxes, or solar proton energies; sequence numbers range from 1 to 5 (in the solar proton sections, 1 to 4).

See Table 4 for a description of the punched output.

If the "Solar Proton Module" was not included in the run, or if the trajectory was completely shielded geomagnetically, no cards for solar protons are punched.

#### Output-Tables Module 1

When the program is used in its simplest form, this module should be included if tabular output is desired. It produces a composite orbit spectrum table, containing:

- Integral energy levels, in MeV,
- Average orbit integrated spectrum, in particles per square centimeter per second,

- 3. Difference flux, in particles per square centimeter per second per  $\Delta E$ , and
- 4. A column labelled "differential flux", which contains only zeroes.

When the "Differential Spectrum Module" is included and if there are ten or more non-zero elements given in the integral spectrum, items (1), (2), and (3) remain the same, but (4) now contains average differential flux values, in units of particles per square centimeter per second per keV.

For more information on the calculation of either of these fluxes, see the section on "Method".

This module also prints two additional, independent tables for (a) the exposure index, and (b) the solar proton results. The exposure index table presents in the first column the intensity ranges, in the second column the total duration of trajectory exposure to each intensity range, and in the last column the total number of particles encountered while so exposed. The solar proton table lists in the header the mission duration TAU, the confidence level Q, the number of anomalously large events NALE predicted for TAU and Q, and the geomagnetically determined exposure factor used in the calculations, and presents two columns containing respectively the energy levels in MeV, and the total fluence per square centimeter for each energy,

If the "Solar Proton Module" and/or the "Exposure Index Module" have not been included in the run, then the corresponding tables do not appear in the print out.

If no tabular output is required, delete the "Output-Tables Module 1".

#### Output-Tables Module 2

This module prints the results calculated in the "Peaks-per-Orbit Module". There are nine columns on this table. Column 1 is an orbit counting device, based on the period of the orbit. Column 2 gives the absolute instantaneous peak flux encountered during that orbit. Columns 3, 4, and 5 indicate the spacecraft position in geocentric coordinates at which the peak was encountered, while columns 6, 7, and 8 denote respectively the time and the magnetic B-L coordinates for this event. Finally, the last column indicates the total flux encountered during that particular orbit. It is advisable to disregard the last line on this table because many times that orbit is incomplete and the fluxes or positions shown do not correspond to true peaks.

#### BLOCK 6: Program Termination

In Block 6, the program returns to the beginning of BLOCK 1 where it checks whether there is another trajectory to be processed. If no other trajectory is to be processed, the run terminates. No user action is necessary.

#### **ACKNOWLEDGEMENTS**

We wish to thank Drs. R. Hilberg and M. Teague for many helpful discussions and constructive suggestions.

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Table 1
Running Times of SOFIP for 720 Input Positions on the IBM 360/91 Computer

	Compile	Link	Execute	Total
<u>Protons</u>				
Stripped	.06/.03	.00/.14	.06/.04	.12/.21
A11	.11/.04	.00/.18	.08/.06	.19/.28
<u>Electrons</u>				
Stripped	.06/.03	.00/.15	.06/.04	.12/.22
A11	.11/.04	.00/.18	.09/.06	.20/.28

Times are given in decimal minutes. The first figure in each entry is for CPU, and the second is for I/O. Values are averages of three runs for each type and species.

Table 2 Core Requirements for SOFIP

	Core required for source program (in 1000 bytes)
SOFIP+	
Stripped	11.8
All Modules	16.8
TRARA1+	1.5
TRARA2+	2.5
SOLPRO+	2.4
DSPCTR+	8.4
FORTRAN Library Functions	
Stripped	22.7
All Modules	24.6
Environment Models*: For proton runs	26.1 or 26.8
For electron runs	35.6 or 37.3
See table below for size of individual models	
AP8MAC	26.1
AP8MIC	26.8
AE 17HI	17.5
AE 17LO	15.8
AE 6MAX	19.8
AE 5MIN	19.8

<sup>\*</sup>Compiled under FORTRAN G
\*Compiled under FORTRAN H
If SOFIP with all modules, TRARA1, TRARA2, SOLPRO, and DSPCTR are
compiled under FORTRAN H, the results will be a total of 3.3K less than these.

TABLE 3

Input Parameters: Description and Format

Card	Columns	Format	Name	Description
1	1-12	3A4	NAME*	Any 12-character alphanumeric description of vehicle or orbit
	20-22	13	INCL*	Approximate orbit inclination in degrees
† 1	30-35	16	I PRG*	Approximate orbit perigee in kilometers
	40-45	16	I APG*	Approximate orbit apogee in kilometers
	50-51	12	MODEL*	Number of field model (from ALLMAG <sup>8</sup> ) used in calculation of magnetic parameters B and L in conversion of trajectory ephemeris
	60-68	F9.6	PERIOD	Mathematical period of orbit in decimal hours
	70-76	F7.2	BLTIME*	Epoch for which the coefficients of the field model were evaluated for the B-L calculations, in decimal years A.D.
2	1-2	12	NRGYLV	Threshold energy selector for running printout, exposure index, and peaks
	10-13	14	ITAPE*	Orbit tape identifier
	20-21	12	NTABLS	Number of copies of tables to be produced
	30-35	F6.2	CUTOFF	Orbit time (in decimal hours) at which run is to be terminated
	40-41	12	ISKIP	Program will process only every ISKIPth point on trajectory tape. ISKIP=1, all points are processed.
Towns the state of	50-51	12	KPRINT	The "Running-Printout-Module", if included in the run, will print only every KPRINTth point of the trajectory points read. Note: KPRINT=O will cause the program to abend.

Format of input: (3A4,7X,13,7X,16,4X,16,4X,12,8X,F9.6,1X,F7.2 /12,7X,14,6X,12,8X,F6.2,4X,12,8X,12)

<sup>\*</sup>Starred quantities are not required for calculations, but are used only for labelling output.

TABLE 4
Punched Output: Description and Format

Card	Variable(s) Format	Comments	
1	NAME(3),INCL,IPRG, 3A4,1X,12,'/',15,'-	APG,MODEL,BLTIME -',I6,1X,'I(#/CM**2-SEC) D(#/CM**2-SEC-KEV) MOD/TM=',I1,'/',F6.1	
		Header card containing vehicle identification*, inclination*, perigee*, apogee*, the units of the differential and integral fluxes which are to to be punched, and the model number (from ALLMAG <sup>8</sup> ) and epoch for which the B and L of the trajectory tape were calculated*.	
2-6	ENERGY(30,ITYPE) 1P6E12.4	The 30 integral threshold energies, in MeV, for the particle species considered in this run.	
7-11	AIFLXS(30) 1P6E12.4	The orbit integrated, integral fluxes for the 30 energy levels punched previously, averaged into units of particles/cm²·sec.	
12-16	DIFSPC(30) 1P6E12.4	The differential fluxes obtained from the preceeding integral spectrum in units of particles/cm²·sec·keV. Zeros will be punched if the "Differential Spectrum Module" was omitted.	
17	IQ,T,INALE,EXPFCT 'SOLAR PROTONS #EN	HERGIES=20 Q=',12,' TAU=',F4.1,' NALE=',I1,' EXPFCTR=',F5.2	
i.		Header card giving the number of Solar Proton energy levels processed, and containing confidence level Q, mission duration tau, number of AL events for given Q and tau, and geomagnetic shielding effect in the form of an exposure factor.	
18-21	SPNRG(20) 1P5E12.4	The 20 integral threshold energies, in MeV, for the solar flare protons.	
22-25	F(20) 1P5E12.4	The total unattenuated interplanetary solar flare proton fluences for the preceeding integral spectrum, modified by the exposure factor punched above, and for the Q and tau given in the solar proton header card, in units of particles/cm <sup>2</sup> .	

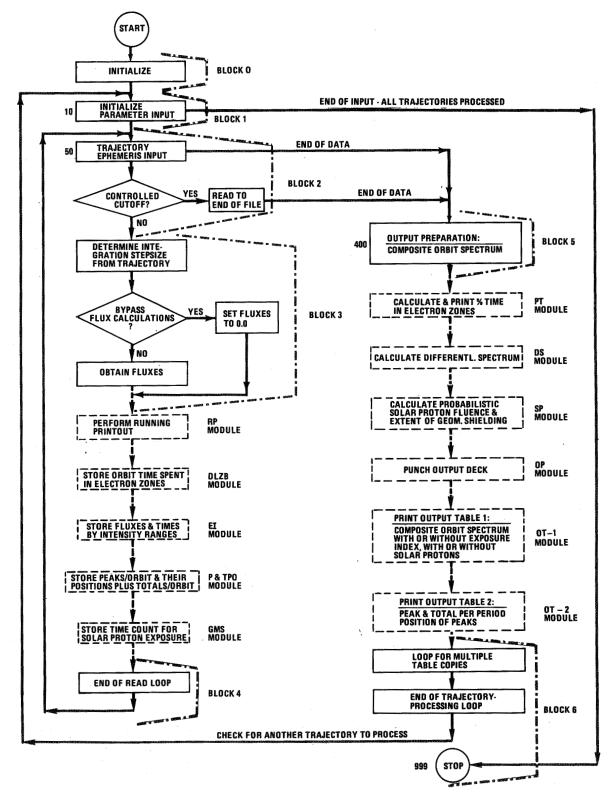
\*taken directly from input

## FIGURE 1: MODULAR STRUCTURE AND ARRANGEMENT OF SOFIP

-2/2-2/4/	
BLOCK O INITIALIZATION OF PROGRAM	38-88
BLOCK 1 INITIALIZATION OF DATA PARAMETER INPUT	89-130
BLOCK 2 INPUT POSITIONAL DATA FROM TAPE (TRAJECTORY)	131-146
BLOCK 3 OBTAIN FLUXES PERFORM CALCULATIONS	147-174
RUNNING PRINTOUT MODULE PRINT POSITIONAL DATA	175-192
ORBIT L-ZONE BREAKDOWN MO COUNT TIMES EACH ZONE IS VISITED	<b>DULE</b> 193-201
EXPOSURE INDEX MODULE STORE FLUXES AND TIMES BY INTENSITY RANGES	202-213
PEAKS PER ORBIT MODULE DETERMINE PEAKS AND POSITION, PLUS TOTAL, PER PERIOD	214-237
GEOMAGNETIC SHIELDING MODU DETERMINE WHETHER POSITION IS GEOMAGNETIC- ALLY SHIELDED (STEP COUNT FOR L <5)	JLE 238-240
BLOCK 4 END OF READ LOOP	241-243
1	

/	
BLOCK 5 OUTPUT PREPARATION	244-254
PERCENT TIME MODULE CALCULATE PERCENTAGE OF TOTAL TIME SPENT IN EACH ZONE	255-271
DIFFERENTIAL SPECTRUM MO CALL SUBROUTINE DSPCTR	<b>DULE</b> 272-273
SOLAR PROTON MODULE CALL SUBROUTINE SOLPRO	274-287
OUTPUT PUNCH MODULE PUNCH INTEGRAL AND DIFFERENTIAL SPECTRA, SOLAR PROTONS	288-307
OUTPUT MODULE TABLE 1 WITH ORBIT INTEGRATED SP AND WITH OR WITHOUT DIFF SPECTRUM AND/OR EXPOSUR AND/OR SOLAR PROTONS	FERENTIAL
OUTPUT MODULE TABLE 2 PEAKS AND POSITION PLUS TOTAL PER PERIOD	382-396
BLOCK 6 PROGRAM TERMINATION	397-401

#### FIGURE 2: FLOW DIAGRAM FOR SOFIP



```
FOR USE WITH NSSDC'S STANDARD ENVIRONMENT MODELS *******SOFTPOG3
** DESIGNED AND TESTED BY STASSINOPOULOS, HEBERT, BUTLER, & BARTH
                                                            **SOFTP005
  CODE 601, NASA/GODDARD SPACE FLIGHT CENTER: GREENBELT, MD. 20771 **SOFIP006
** SINGLE PRECISION DECK FOR FORTRAN IV (EBCDIC+029 PUNCH)
                                                            **SOFTPOOT
** TRAJECTORY INPUT FROM UNFORMATTED BINARY OR BCD FORMATTED TAPE
                                                            **50FTP008
***
                                                              50FIP010
    INPUT PARAMETERS:
***
                                                              SOFIPO11
***
    * NAME : 12-CHARACTER MISSION (OR PROJECT) NAME
                                                              SOFT PO12
           : APPROXIMATE INCLINATION OF ORBIT PLANE IN DEGREES (1*4)SOFTP013
***
    * INCL
          : APPROXIMATE PERIGEE ALTITUDE IN KILOMETERS
    * IPRG
                                                          ([*4)50FTP014
ale ale ale
          : APPROXIMATE APOGEE ALTITUDE IN KILOMETERS
***
    * IAPG
                                                          ([*4)SOF[PO15
***
    * MODEL : NUMBER OF FIELD-MODEL USED IN B/L CALCULATION
                                                          (R*4) SOFTP016
***
    * PERIOD: MATHEMATICAL PERIOD OF ORBIT IN HOURS
                                                          (R*4) SOFTPO17
***
    * BLTIME: EPOCH OF FIELD-MODEL USED IN B/L CALCULATION
                                                          (R*4)50FIP018
    * NRGYLV: THRESHOLD-ENERGY SELECTOR FOR RUNNING PRIMIDUT
***
                                                          (1*4)SDFTP()19
    * ITAPE : B/L ORBIT TAPE IDENTIFIER, < 10000
                                                          (1*4)SOFIPO20
***
    * NTABLS: # OF OUTPUT-TABLE SETS PER TRAJECTORY
                                                          ( ] *4 ) SOF JPO 21
冰冰冰
***
    * CUTOFF: ORBIT DURATION IN DECIMAL HOURS
                                                          (R*4)50FIP022
***
    * ISKIP : POSITION SKIPPING CONTROL
                                                          ( ] *4 ) SOF I PO 23
    * KPRINT: RUNNING PRINTOUT CONTROL
                                                          (T*4)SOFTP024
***
                                                              SOF IPO25
***
    INPUT VARIABLES:
                                                              SUFTP026
***
              POSITIONAL TIME (DECIMAL HOURS)
本本本
    * PSNTIM:
                                                              SOFTP027
    * PSNLON:
                 11
                        LONGITUDE (DEGREES)
                                                              SOFTP028
***
    * PSNLAT:
                  11
                        LATITUDE (DEGREES)
                                                              SOFTPOZO
    * PSNALT:
                 **
                        ALTITUDE (KILOMETERS)
                                                              SOFIPO30
***
    * PSNB :
                        FIELD MAGNITUDE (GAUSS)
                                                              SOFTP031
    * PSMI
                 11
***
          •
                        SHELL PARAMETER (EARTH RADII)
                                                              SOFTP032
********************
*** TO READ BCD FORMATTED ORBIT TAPES, UNCOMMENT LINES 132,137,8 143. SOFTPO34
*** COMMENT OUT LINES 133-134,138-139,8 144.
                                                              SOFTP035
*** TO READ UNFORMATTED BINARY ORBIT TAPES. UNCOMMENT LINES 133-134.
                                                              SOFIP036
*** 138-139.& 144. COMMENT OUT LINES 132.137.8 143.
                                                              SOFTP037
*** ***************** BLOCK O: INITIALIZATION ********************
   COMMON /AP8MAC/DESCR(8).LIST(1)
                                                              SOFTP039
   COMMON /AE6MAX/DESCR(8), LIST(1)
                                                              SOFIPO 40
   COMMON /AEI7HI/DESCR7(8), LIST7(1)
                                                              SOF1P041
   COMMON /AEI7LO/DESCR7(8).LIST7(1)
                                                              SOFIPO42
   COMMON /AE5MIN/DESCR(8), LIST(1)
                                                              SOF IPO 43
```

```
COMMON /APSMIC/DESCR(8), LIST(1)
                                                                    SOFIP044
 REAL MODLAB*8(4.7)/ HENDRICK!, 'S&CAIN 9', '9-TERM G', 'SEC 9/65', ' CSOFTPO45
*AIN FT', '.AL. 120', '-TERM GS', 'FC 12/66', ' CAINSLA', 'NGEL 143', '-TSDFIP046
*ERM PD!, 'GD 10/68'. CAINESW!, 'EENEY 12'. 'O-TERM P!, 'DGD 8/69', '
                                                                    SOFTP047
   IGRE!.! 1965.0 !.!80-TERM !,!10/68
                                        ... LEATON .. MALIN EV. . LANSOFIPO48
$$ 80-T', ERM 1965', 1
                        HURWI', 'TZ US C&', 'GS 168-T', 'ERM 1970'/,
                                                                    SHFIP049
$MODURE*8(4), AP8/! AP8//, MAX/!MAX !/, MIN/!MIN !/, LOW/'S LO!/,
                                                                    SOF1P050
SMAC/'MAC'/,DESCR7(8).BINDMY*8(5),ADUMMY(6).MOD7/'LO-7'/
                                                                    SOFTP051
 REAL EMERGY(31,2)/2.,3.,4.,5.,6.,8.,10.,15.,20.,25.,30.,35.,40.,
                                                                    SOFTP052
 $45.,50.,55.,60.,70.,80.,90.,100.,125.,150.,175.,200.,250.,300.,
                                                                    SOFTP053
                                                                    SOFIPO54
.5350.,400.,500.,0.,.1..2,.3,.4,.5,.6,.7,.8,.9,1.,1.25,1.5,1.75,2.,
 52.25,2.5,2.75,3.3.25,3.5,3.75,4.,4.25,4.5,4.75,5.,5.5,6..6.5,7.,
                                                                    SCFIP055
$0.0/,SPNRG(20)/10.,20.,30.,40.,50.,60.,70.,80.,90.,100.,110.,120.,SOF1P056
                                                                    SOFIPO57
 5130..140..150..160..170..180..190..200./
                                                                    S0F1P058
 INTEGER NRGRNG(10,2)/1,3,5,7,12,20,22,26,30,31,1,5,8,10,12,13,14,
 $22.30.31/,IZONE(120)/10*1.17*2.93*3/,NRBITO/1/
                                                                    SOFTP059
 DIMENSION FLUXES(30).ALGFLX(30).ALMFLX(30).DIESPC(30).EXPFLX(10).
                                                                    SOFIPO60
                                                                    SOFTPO61
 *PKVALU(50,8).AIFLXS(30).ENRMGS(11).EXPTIM(10).IYMD(3).LCOUNT(4).
 SDIFFLX(30), NAME(3), PKFLX(50), PKTIM(50), PTIME(4),
                                                                    SOFIPO62
 *PKLON(50),PKLAT(50),PKALT(50),PKB(50),PKL(50),TAUFLX(50),F(20)
                                                                    SOFTP063
 EQUIVALENCE(PKVALU(1.1).PKFLX(1)).(PKVALU(1.2).PKLON(1)).(PKVALU(1SOFIPO64
 *,3),PKLAT(1)),(PKVALU(1,4),PKALT(1)),(PKVALU(1,5),PKTIM(1)),(PKVALSOFIPO65
 SU(1,6),PKB(1)),(PKVALU(1,7),PKL(1)),(PKVALU(1,8),TAUFLX(1))
                                                                    SOFIP066
 REAL TYPLBL(3,2)/' PR', OTON', 'S ', 'ELEC', 'TRON', 'S HI'/,
                                                                    SOFTP067
 $FIRNGS(11)/!0.E0!,!1.E0!,!1.E1!.!1.E2!,!1.E3!,!1.E4!,!1.E5!,
                                                                    50FTP068
 s'1.66','1.67','OVER',' '//XLABEL*8(3,2)/'PRNRGY','PRINTG','PRDIFF'SOFIPO69
*,'ELNRGY','ELINTG','ELDIFF'/,PROTLB*8(2)/'SPNRGY','SPFLUX'/
                                                                    S0F1P070
1 FORMAT('IMAME = '.3A4/' INCL = '.13/' IPRG = '. 16/' IAPG = '. SOFIPO71
SI6/! ITAPE = '.14/! MODEL = '.12/! PERIOD= '.F9.6/
                                                                    S0F1P072
 s' BLTIME= ',F7.2/' NRGLEV= ',I2/' ΝΤΔΒLS= ',I2/' CUTOFF= ',F6.2/
                                                                    SOFTP073
s' ISKIP= ', I2/' KPRINT= ', I2//)
                                                                    SOFTP074
2 FORMAT('1',131('*')/' * SOFIP : SHORT ORBITAL FLUX INTEGR. PROGRAMSOF1P075
 $ FOR STANDARD ASSDC PROTON AND ELECTRON ENVIR. MODELS (SPECIES CONSOFIPO76
 SSIDERED SEPARATELY) *'/' * MAGNETIC PARAMETERS B AND L COMPUTED WISOFIPO77
 STH GEOMAGN. FIELD MODEL!, I3. !: !, 4A8. ! * COEFF. UPDATED TO: !, F7.1. SOFIPO78
 *BOG=',I6,'KM * B/L TAPE=TD',I4,' * PERIOD=',F7.3,'HRS * SOLAR ',A3,SOFIPORO
            *'/' * FOR INFORMATION OR EXPLANATION CONTACT F.G. STASSSOFIPO81
 $INOPOULOS AT NASA-GSEC, CODE 601, GREENBELT, MARYLAND 20771, TEL. (350FIP082
                                                                    SHFTP083
 $01)-344-8067 *1/1X.131(!*1)//)
3 FORMAT(2('1'/12('0'/)/53x,28('*')/53x,'**',6X,3A4,6X,'**'/53x,'**'SOFIPO84
 $, I3, 'DEG/', I5, 'KM/', I6, 'KM **'/53X, 28('*')/))
                                                                    SOFTP085
4 FORMAT (3A4,7X,13,7X,16,4X,16,4X,12,8X,F9,6,1X,F7,2/12,7X,14,
                                                                    SDFIP086
 $6X, I2, 8X, F6, 2, 4X, I2, 8X, I2)
                                                                    SOFIP087
5 FURMAT (6E18.8)
                                                                    SOFTPORR
```

```
C *** ******************* BLOCK 1: INITIALIZATION ****************
   10 READ(5,4,END=999) NAME, INCL, IPRG, IAPG, MODEL, PERIOD, BLTIME, NRGYLY, SOFIPO90
     *ITAPE.NTABLS.CUTOFF.ISKIP.KPRINT
                                                                       SOFTP091
                                                                       SOFIP092
      WRITE(6,3) (NAME.INCL.IPRG.IAPG.I=1,2)
                                                                       SOFIP093
     NURBIT=1
                                                                       SOFTP094
      IPASS=1
                                                                       SOF IPO95
     IPRINT=<PRINT
                                                                       SOFIP096
      ASSIGN 110 TO MG02
                                                                       SOFTP097
     \mathbf{L} = ()
                                                                       SOFIP098
     LSUM=0
                                                                       SOFIP099
     EXPECT=0.0
                                                                       SOFTP100
     XAMNIM=MAX
                                                                       SOFIP101
     ISWTCH=1
                                                                       SOFIP102
      IF (DESCR(1).EQ. 4P8) GO TO 15
                                                                       SOFIP103
     ITYPF = 2
                                                                       SOFIP104
      ASSIGN 120 TO NGO2
                                                                       SOFIP105
      IF(DESCR(2).NE.MAX) XAMNIM=MIN
                                                                       SOFIP106
      IF(DESCR7(2).EQ.MOD7) TYPLBL(3,2)=LOW
                                                                       SOFTP107
     GO TO 17
                                                                       SOFTP108
   15 IF(DESCR(2).NE.MAC) XAMNIM=MIN
                                                                       SOFIP109
   17 PO 20 I=1.4
                                                                       SOFIP110
      LCOUNT(I)=0
                                                                       SOFIP111
   20 MODUBU(I) = MODUAB(I.MODEL)
                                                                       SOFIP112
      TAU = PERIOD
                                                                       SOFIP113
     FLXSUM = 0.0
                                                                       SOFIP114
     OFLXSM = 0.0
                                                                       SOFIP115
     PE\Delta K = -1.0
                                                                       SOFIP116
     DO 30 MRNG=1,10
                                                                       SOFIP117
     ENRNGS(NRNG) = ENERGY(NRGRNG(NRNG,ITYPE),ITYPE)
                                                                       SOFIP118
     EXPTIM(NRNG) = 0.0
                                                                       SOFIP119
  30 EXPELX(NRNG) = 0.0
                                                                       SOFIP120
     DO 35 NRGSP=1.20
                                                                       SOFIP121
   35 F(NRGSP)=0.0
                                                                       SOFIP122
      DO 40 NRG=1,30
                                                                       SOFIP123
     AIFLXS(NRG) = 0.0
                                                                       SOFIP124
      ALNFLX(NRG) = 0.0
                                                                       SOFTP125
     DIESPC(NRG) = 0.0
                                                                       SOFIP126
  40 \text{ FLUXES(NRG)} = 0.0
                                                                       SOFTP127
C *** WRITE OUT INPUT PARAMETERS
                                                                       SOFTP128
     WRITE(6.1)NAME, INCL, IPRG, IAPG, ITAPE, MODEL, PERIOD, BLTIME, MRGYLV,
                                                                       SOFTP129
    SNIABLS, CUTOFF, ISKIP, KPRINT
                                                                       SOFTP130
 C
     READ(9,5,END=400,ERR=10)PSNTM1,PSNLM1,PSNLT1,PSNAL1,PSNB1,PSNL1
                                                                       SOFIP132
      READ(9.END=400.ERR=10)PSNTMl.PSNLNl.DUMMY,PSNLT1.DUMMY,PSNALl.
                                                                       SOFIP133
```

	5	DUMMY, PSNB1, DUMMY, PSNL1, DUMMY	SOFT P134
		TMLAST = PSNTM1	SOFTP135
	50		SHETP136
С			SCFIP137
			SHFIP138
	5	BDUMMY.PSNB.DUMMY.PSNL.DUMMY	SOFTP139
			SOFIP140
		IF(PSNTIM.LE.CUTOFF) GO TO 65'	SOFTP141
С	* * *	DUMMY READ LOOP TO READ TO END OF FILE	SOFIP142
С	66	READ(9,5,END=400,ERR=10) ADUMMY	S0F1P143
	66	READ(9, END=400, ERR=10) BINTIM, BINDMY	SOFIP144
		GO TO 66	SOFTP145
		CONTINUE	SOFTP146
		******************* BLOCK 3: CALCULATIONS ************	SOFTP147
С	***	CALCULATE KPSTEP (NUMBER OF MINUTES BETWEEN POINTS ON B/L TAPE)	SOFIP148
		GO TO (70,80), IPASS	SOFIP149
	70	KPSTEP = INT((PSNTIM-TMLAST)/.0166667+0.1)	SOFIP150
		TMLAST = PSNTIM	SOFTP151
С	***		SOFTP152
		IF(PSNL.GT.0.0.AND.PSNL.LT.12.0) GO TO NGO2,(110,120)	SOFTP153
		DO 100 NRG=1,30	SOFTP154
	100	FLUXES(NRG) = 0.0	SOFTP155
		GO TO 170	SOFIP156
		OBTAIN COMMON LOGARITHM OF POSITIONAL FLUXES (ALGELX)	SOFTP157
С		PROTONS	SOFIP158
	110	CALL TRARA1(DESCR.LIST.PSNL.PSNB.ENERGY(1,1).ALGFLX(1).30)	SOFIP154
^	V- V- V-	GO TO 140	SOFTP160
U		ELECTRONS  JELINITARIO CARRENTES AND LE 2000 CO. TO. 120	SOFTP161
	120	IF(INT(100.0*PSNL+0.2).LE.280) GO TO 130 CALL TRARAI(DESCR7.LIST7.PSNL.PSNB.ENERGY(1,2).ALGFLX(1).30)	SOFIP162
		GO TO 140	SOFIP163
	120	CALL TRARAI(DESCR.LIST. PSNL.PSNB.ENERGY(1,2),4LGFLX(1),30)	SOFTP164 SOFTP165
_		CONVERT LOG-FLUX TO FLUX	SOFTP165
U		DO 150 NRG=1,30	SOFTP167
	140	FLUXES(NRG) = 10.0**ALGFLX(NRG)	SOFTP168
	150	IF(FLUXES(NRG).LT.1.001) FLUXES(NRG) = 0.0	SOFIP169
r		SUM FLUXES FOR (A) RUNNING PRINTOUT, (B) TABULAR OUTPUT	SOF 19170
Ü		FLXSUM = FLXSUM+FLUXES(NRGYLV)*FLOAT(KPSTEP)*60.	SOFTP171
		DO 160 NRG=1.30	SOFTP172
	160	AIFLXS(NRG) = AIFLXS(NRG)+FLUXES(NRG)	SOFTP173
		CONTINUE	SOFTP174
C		**************************************	
		GO TO (200,210), IPASS	SOFTP176
	200	WRITE (6,2) MODEL, MODEL BLTIME, NAME, INCL, IPRG, IAPG, ITAPE, PERIOD.	
		BXAMNIM	SOFIP178

```
WRITE (6,201)(TYPLBL(I.ITYPE), I=1.3), ENERGY(NRGYLV, ITYPE)
                                                                    SOFTP179
 201 FORMAT( *0 *, 21X , ***** * * * * * * * * G9 . 3 . * MEV)
                                                 *****
                                                               LONGSOFTP180
          LAT.
                 ALT.
                       FIELD
                                LINE ORBIT
                                                POSITIONAL
                                                          TIME-INTESOFIP181
    $ .
                                           TIME
          ORBITAL!/! '.T28.!-8-!.T37.!-L-
                                                     FLUX
                                                              PSTML SOFIPLAZ
    $G
            FLUX(SUM)!/! (DEG)
                                 (DEG)
    $FLUX
                                         (KM) (GAUSS) (F.R.)
                                                              (HRS)SDF1P183
        #/CM**2/SEC!)
                                                                    SOFTP184
     WRITE(6,202)PSNTM1,PSNLN1,PSNLT1,PSNAL1,PSNR1,PSNL1
                                                                    SUFTP185
 202 FORMAT( * *,T41,F9.5,T2,F7.2,1X,F6.2,1X,F8.1,1X,F8.5,1X,F5.2,T50,
                                                                    SOFTP186
    $7(2X,1PE10.3))
                                                                    SOFTP187
 210 IF(MOD(IPRINT, KPRINT), NE. 0) GO TO 220
                                                                   SOFIPLAR
     TIFLUX = FLUXES(NRGYLV)*FLOAT(KPSTEP)*60.
                                                                    SOFTP189
     WRITE(6,202) PSNTIM, PSNLON, PSNLAT, PSNALT, PSNB, PSNL;
                                                                    SOFTP190
    SFLUXES(NRGYLV).TIFLUX.FLXSUM
                                                                    SOFTP191
                                                                   SOFIP192
 220 IPRINT=IPRINT+1
 *** ****** THIS MODULE MUST BE USED WITH PERCENT TIME MODULE ******OFIP194
C *** STORE TIME IN INNER & OUTER ZONE, EXTERNAL
                                                                    50FJP195
     IF(PSNL.LT.0.0.0R.PSNL.GT.11.0) GO TO 250
                                                                    SOFIP196
     IZ = IZONE(INT(PSNL/.1))
                                                                    S0F1P197
     LCOUNT(IZ) = LCOUNT(IZ) + 1
                                                                    S0FTP198
                                                                    SOFTP199
     GD TD 260
 250 LCOUNT(4) = LCOUNT(4)+1
                                                                    SOFTP200
 260 CONTINUE
                                                                    S0FT9201
C *** STORE FLUXES AND TIMES IN INTENSITY RANGES
                                                                    SOFIP203
     GO TO(270,280), IPASS
                                                                    SOFTP204
                                                                    SOFTP205
 270 ISWTCH=ISWTCH+1
                                                                    SOFTP206
 280 INTRNG = (8-INT(1.0-SIGN(0.5, ALGFLX(NRGYLV)-7.0)) *
                                                                    SOFTP207
    $(7-INT(ALGFLX(NRGYLV)))) * INT(1.0+SIGM(0.5,
                                                                    S0FTP208
    $FLUXES(NRGYLV)-1.0009))+1
     EXPELX(INTRNG)=EXPELX(INTRNG)+FLUXES(NRGYLV)*60.0*FLOAT(
                                                                    S0F1P209
    SKPSTEP)
                                                                    SOFIP210
     EXPFLX(10)=EXPFLX(10)+FLUXES(NRGYLV)*60.0*FLOAT(KPSTEP)
                                                                    SOFTP211
                                                                    SOFTP212
     EXPTIM(INTRNG) = EXPTIM(INTRNG) + FLOAT(KPSTEP) * .0166667
     EXPTIM(10) = EXPTIM(10) + FLOAT(KPSTEP) * .0166667
                                                                    SOFIP213
C *** *********** PEAK AND TOTALS PER ORBIT MODULE ***************
C *** DETERMINE ORBIT NUMBER AND TOTAL FLUXES PER ORBIT
                                                                    SOFTP215
                                                                    SOFTP216
     IF(PSNTIM.LT.TAU) GO TO 300
                                                                    SOFIP217
     PEAK = -1.0
     TAUFLX(NORBIT) = FLXSUM-OFLXSM
                                                                    SOFIP218
                                                                    SOFJP219
     OFLXSM = FLXSUM
     NRBITO=NORBIT
                                                                    SOFTP220
     NORBIT = NORBIT+1
                                                                    SOFTP221
     TAU = NORBIT * PERIOD
                                                                    SOFTP222
     IF(NORBIT.LE.50) GO TO 300
                                                                    SOFIP223
```

```
SOFTP224
     WRITE(6,301)
 301 FORMAT("OERROR: NORBIT EXCEEDS LIMIT OF 50. ****************
                                                                   SOFIP225
                                                                   SOFTP226
C *** DETERMINE FLUX PEAKS AND POSITIONS PER ORBIT
                                                                   SOFIP227
 300 IF (FLUXES (NRGYLV).LE.PEAK) GO TO 310
                                                                   SOFIP228
                                                                    SOFIP229
     PKFLX(NORBIT) = FLUXES(NRGYLV)
     PKTIM(NORBIT) = PSNTIM
                                                                   SOFIP230
     PKLOM(NORBIT) = PSNLON
                                                                    SOFIP231
     PKLAT(NORBIT) = PSNLAT
                                                                    SOFTP232
     PKALT(NORBIT) = PSNALT
                                                                    SOFTP233
     PKB(NORBIT) = PSNB
                                                                    SOFIP234
                                                                    SOFTP235
     PKL(NORBIT) = PSNL
     PEAK = FLUXES(NRGYLV)
                                                                   SDFIP236
                                                                   SOFIP237
 310 CONTINUE
C *** ****** THIS MODULE MUST BE USED WITH SOLAR PROTON MODULE ******SOFIP239
     IF (INT (PSNL).GE.5.OR.PSNL.LE.0.0) L=L+1
                                                                   SOFTP240
C *** ********* BLOCK 4: LOOPING (READ-LOOP ENDS HERE) *************OFIP241
                                                                    SOFTP242
     IPASS=2
                                                                    SOFTP243
     GO TO 50
C *** COMPOSITE ORBIT SPECTRUM
                                                                    SOFIP245
                                                                    SOFIP246
 460 AFCTRS = (KPSTEP*1440.0) / (PSNTIN*86400.0)
     DO 410 NRG=1.30
                                                                    SOFIP247
     AIFLXS(NRG) = AIFLXS(NRG)*AFCTRS
                                                                    SOFTP248
                                                                    SOFIP249
     IF(AIFLXS(NRG), LE, 0, 0) GO TO 440
     ALNELX(NRG) = ALOG(\Delta IELXS(NRG))
                                                                    SOFTP250
 410 CONTINUE
                                                                    SOFTP251
                                                                   SOFIP252
 440 DU 450 NRG=1,29
                                                                    SOFIP253
  450 DIFFLX(NRG) = AIFLXS(NRG)-AIFLXS(NRG+1)
     DIFFLX(30) = AJFLXS(30)
                                                                    SOFIP254
C *** ************************ PERCENT TIME MODILE *********************
C *** ** THIS MODULE MUST BE USED WITH ORBIT L-ZONE BREAKDOWN MODULE  **SOFIP256
C *** CALCULATE AND PRINT PERCENT TIME TABLE
                                                                    S0F1P257
                                                                    SOFIP258
     LSUM=LCOUNT(1) + LCOUNT(2) + LCOUNT(3) + LCOUNT(4)
                                                                    SOFIP259
     IF(LSUM.EQ.O) GO TO 470
                                                                    SOFIP260
     DO 460 IL=1.4
  460 PTIME(IL)=FLOAT(LCOUNT(IL)*KPSTEP)*1.666667/TMLAST :
                                                                    SOFTP261
     PTIZ=PTIME(1)+PTIME(2)
                                                                    S0FTP262
     WRITE(6,401)PTIZ, (PTIME(II), II=1,4), PSMTIP
                                                                    SOFTP263
 470 CONTINUE
                                                                    SOFTP264
  401 FORMAT( *0***** PERCENT OF TOTAL LIFETIME SPENT INSIDE AND OUTSIDE SOFIP265
     STRAPPED PARTICLE RADIATION BELT ****'//6X,'INNER JONE (1.0 <= L < SOFIP266
     $2.8) : ',F6.2.' %'/18X,'OUTSIDE TRAPPING REGION (1.0 <= L < 1.1) SOFIP267
     5: '.F6.2,' %'/18x,'INSIDE TRAPPING REGION (1.1 <= L < 2.8) :.', SOFIP268
```

```
SE6.2, * *'/6X, 'OUTER ZONE (2.8 <= L <= 11.0) : ', F6.2, * *'/6X, *EXTESOFIP269
            (L > 11.0)
                              : '.F6.2, ' %'//' TOTAL ORBIT TIME IS : ', SOFIP270
    SRNAL
    *FR.2, | HOURS!)
                                                                     ShFTP271
C *** ************** DIFFERENTIAL SPECTRUM MODULE ******************************
     CALL DSPCTR(ALNFLX(1).EMERGY(1.ITYPE).DJFSPC(1))
                                                                     SOFTP273
C *** **** THIS MODULE MUST BE USED WITH GEOMAG. SHIELDING MODULE ****SOFIP275
     T=12.
                                                                     SOFTP276
     I = T
                                                                     SOFTP277
     J(0=90)
                                                                     SOF 1 P 2 78
     ISWTCH=ISWTCH+2
                                                                     SOFIP279
     IF(L.LE.O) GO TO 510
                                                                     SOFIP280
     CALL SOLPRO(T.ID.F.INALE)
                                                                     SOFTP281
     EXPUTM=FLOAT(L*KPSTEP)*.0166667
                                                                     SOFTP282
     EXPECT=(EXPOTM/PSNTIM)
                                                                     SOFIP283
     DO 500 J=1,20
                                                                     SOFIP284
     F(J)=F(J)*EXPFCT
                                                                     SOFIP285
 500 CONTINUE
                                                                     SOFIP286
  510 CONTINUE
                                                                     SOFIP287
C *** ********************** OUTPUT PUNCH MODULE ******************
C *** PUNCHES ENERGY, INTEG AND DIFF FLUX, SOLAR PROTONS IF PRESENT
                                                                     SOFIP289
     WRITE(7.605) NAME, INCL, IPRG, IAPG, MODEL, BLTIME
                                                                     SOFIP290
     WRITE(7,602)((ENERGY((II-1)*6+JJ,ITYPE),JJ=1,6),XLABEL(1,ITYPE),IISOFIP291
    5, II = 1, 5
                                                                     SOFTP292
     WRITE(7,602)((AIFLXS((II-1)*6+JJ),JJ=1,6),XLABEL(2,ITYPE),II,II=1,SOFIP293
    55)
                                                                     SOFTP294
     WRITE(7,602)((DIFSPC((II-1)*6+JJ),JJ=1,6),XLABEL(3,ITYPE),II,IJ=1,SOFIP295
    55)
                                                                     SOFTP296
     IF(L.LE.O) GO TO 600
                                                                     SOFIP297
     WRITE(7,603) IO.T.IMALE, EXPECT
                                                                     SOFIP298
     WRITE(7,604)((SPNRG((II-1)*5+JJ),JJ=1,5),PROTLB(1),II,II=1,4)
                                                                     SOFIP299
     WRITE(7,604)((F((II-1)*5+JJ),JJ=1,5),PRQTLB(2),II,II=],4)
                                                                     SOFIP300
  600 CONTINUE
                                                                     SOF1P301
 602 FORMAT(1P6E12.4.Δ6.12)
                                                                     SOFIP302
  603 FORMAT( SOLAR PROTONS #ENERGIES=20
                                          Q=1,12,1
                                                   TAU= 1 . F4 . 1 .
                                                                     SOFIP303
     s* MALE=*, I1.* EXPECTR=*.F5.2)
                                                                     SOFIP304
  604 FORMAT(1P5E12.4,12X,A6,I2)
                                                                     SOFIP305
  605 FORMAT(3A4.1X,12,1/1,15,1-1,16,1X,11(#/CM**2-SEC) D(#/CM**2-SEC-KESOFIP306
    SV) MOD/TM=*, I1, */*, F6.1)
                                                                     SOFIP307
DO 900 NTBL=1.NTABES
                                                                     SOFIP309
     WRITE(6,2) MODEL, MODERL, BLTIME, NAME, INCL, IPRG, IAPG, ITAPE, PERIOD,
                                                                     SOFIP310
    SXAMNIM.
                                                                     SOFIP311
     GO TO (710,700,730,720), ISWICH
                                                                     SOFIP312
C *** COMPOSITE ORBIT SPECTRUM AND EXPOSURE INDEX
                                                                     SOF [P313
```

```
700 WRITE (6,701) (TYPLBL(K,ITYPE).K=1,3), ENERGY(NRGYLV.TTYPE).
                                                                        SOFIP314
     $(ENERGY(N,ITYPE),AIFLXS(N),DIFFLX(N),DIFSPC(N),FIRMGS(N),
                                                                        SOFTP315
     $FIRNGS(N+1),EXPTIM(N),EXPFLX(N),N=1,10),(ENERGY(N,ITYPE).ATFLXS(N)SOFTP316
                                                                        SOFTP317
     \$, DIFFLX(N), DIFSPC(N), N=11,30)
  701 FORMAT ("+",41X.16("*"),3X.3A4.2X.16("*")/" ",41X.49("*")///"" SOFIP318
     $T18,15('*'), COMPOSITE ORBIT SPECTRUM ',15('*'),T80,'** FXPOSURE SOFIP319
     $INDEX:ENERGY>'.G9.2.T112.'MEV **'/'0'.T18.'ENERGY
                                                            AVERAGED
                                                                        S0FTP320
                        AVERAGED DIFFE-
                                             INTENSITY
                                                           EXPOSURE
                                                                      TOSOFTP321
         DIFFERENCE
     STAL # OF!/! '.T18. LEVELS
                                 INTEGRAL FLUX
                                                 ENTEGRAL FLUX
                                                                   REMITSOFTP322
                                           ACCUMULATED!/! ',T18,'>(MEV) SOFTP323
     SAL FLUX', 10X, 'RANGES
                                DURATION
                                                             #/CM**2/SECSOFIP324
        #/CM**2/SEC
                        #/CM**2/SEC/DE #/CM**2/SEC/KEV
         (HOURS)
                     PARTICLES!/!0!.T18.0PG9.4.T23.
                                                        1,1PE9.3,7X,
                                                                        SOFTP325
     $1PE9.3,8X,1PE9.3,T81,2A4,T81,'ZERO FLUX',1X,0PF10.3,1X,1PE13.3/8('SOFIP326
     s ',T18,OPG9.4.1PE9.3,7X.1PE9.3.8X,1PE9.3.T81.A4.'-'.A4.lx.OPF10.3.SOFTP327
     SOFTP329
     5,T81,
                TOTAL ', 1X, OPE10.3.1X, 1PE13.3, 20(T18.0PG9.4, 1PE9.3.7X,
     $1PE9.3,8X.1PE9.3/!!))
                                                                        SPETP330
      GO TO 750
                                                                        SOFTP331
C *** COMPOSITE ORBIT SPECTRUM ONLY
                                                                        SOFTP332
  710 WRITE (6.702) (TYPLBL(K.ITYPE),K=1.3).(ENERGY(M.ITYPE),AIFLXS(M).
                                                                        SOF 19333
     sDIFFLX(N).,DIFSPC(N),N=1,30)
                                                                        SOFTP334
  702 FORMAT (*+*,41X;16(***),3X,3A4,2X,16(***)/* *,41X,49(***)///**
                                                                        SHETP335
     *T40.15(!*!), COMPOSITE ORBIT SPECTRUM !.15(!*!)/!0!,T40.!EMERGY
                                                                        SOFIP336
         AVERAGED
                     DIFFERENCE
                                       AVERAGED DIFFE-1/1 1.T40. LEVELS SOFTP337
        INTEGRAL FLUX
                      INTEGRAL FLUX
                                         RENTIAL FLUX:/! '.TAO.'>(MEV)
                                                                        SOFTP338
        #/CM**2/SEC/DE
                                       #/CM**2/SEC/KEV*//30(* *,T41。
                                                                        SOF [P339
     $0PG9.4,T46,1
                      ',1PE9.3,6X,1PF9.3,8X,1PE9.3/))
                                                                        50FTP340
      GO TO 750
                                                                        SOFTP341
C *** COMPOSITE ORBIT SPECTRUM WITH SOLAR PROTONS AND EXPOSURE INDEX
                                                                        50FTP342
  720 WRITE(6,703)(TYPLBL(K,ITYPE).K=1,3),IT.IO.INALE,EMERGY(MRGYLV.
                                                                        50FIP343
     SITYPE), EXPECT, (ENERGY(N.ITYPE), AIFLXS(N), DIFFLX(N), DIFSPC(N), SPARGSOFIP344
     $(N),F(N),FIRNGS(N),FIRNGS(N+1),EXPTIM(N),EXPELX(N),N=1,10),(FNFRGYSOFIP345
     $(N,ITYPE),AIFLXS(N),DIFFLX(N),DIFSPC(N),SPMRG(N),F(N),W=11,20),
                                                                        SOF 1 P346
     5(ENERGY(N,ITYPE),AIFLXS(N),DIFFLX(N),DIFSPC(N),N=21,30)
                                                                        SOFTP347
  703 FORMAT("+",41X,16("*"),3X,3A4,2X,16("*")/" ",41X,49("*")///"0", SOFIP348
     562X, ***** SOLAR PROTONS *****!//63X, *FOR TAU=*, 12, *, 0=*, 12, *: NALE=SOFIP349
     $',I1/3X,15('*'),' COMPOSITE ORBIT SPECTRUM ',15('*'),5X,'WITH GEOMSOFIP350
     *AG SHIELDING + ** EXPOSURE INDEX: ENERGY>+, G9.4, T125. + MEV **!/SOFTP351
     $64X, *(EXPOSE FACTOR= ', F4.2, *) *//3X, *EMERGY
                                                     AVERAGED
                                                                    DIFFSOFTP352
     SERENCE
                 AVERAGED DIFF-
                                                                   INTENSOF [P353
                                      ENERGY
                                                   TOTAL
     $SITY
              EXPOSURE
                         TOTAL # OF 1/3X, LEVELS
                                                                 INTEGRASOFIP354
                                                  INTEGRAL FLUX
     SL FLUX
                RENTIAL FLUX
                                     LEVELS
                                                 FLUENCE
                                                                   RANGESOFTH355
     $5
             DURATION
                        ACCUMULATED 1/3X, 1> (MEV)
                                                   #/CM**2/SEC
                                                                #/CM**2/SOFTP356
     SSEC/DE
               #/CM**2/SEC/KEV
                                     >(MEV)
                                                 #\CM**5
                                                                 */CM**2SOFTP357
     S/SEC
             (HOURS)
                         PARTICLES!//T4,OPG9.4,T9,1
                                                         1,1PF9.3,6X.
                                                                        SPETP358
```

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$1PE9.3,7X,1PE9.3,11X,0PF4.0.7X,1PE9.3,T95.244,T95,'7ER0 FLUX'.
                                                                       SOFTP359
    $0PF11.3.1PE14.3/8(T4.0PG9.4.T9.
                                      1,1PE9.3,6X,1PE9.3,7X,1PE9.350ETP360
    $,11X,0PF4.0,7X,1PE9.3,9X,04,1-1,04.0PF11.3,1PE14.3/),T4,0PG9.4,T9,S0F1P361
             1,1PE9.3.6X,1PE9.3,7X,1PE9.3,11X,0PF4.0.7X,1PE9.3.T95.204. SCFIP362
    51
              TOTAL', OPF11.3, 1PE14.3/10(T4, OPG9.4.T9, ',1PF9.3,6XSOF1P365
    $T95,1
    $,1PE9.3,7X,1PE9.3,11X,0PE4.0,7X,1PE9.3/),10(T4,0PG9.4,T9.
                                                                     1.SDFT0364
                                                                       SHETP365
    $1PE9.3,6X,1PE9.3,7X,1PE9.3/))
                                                                       SOFTP366
     GO TO 750
C *** COMPOSITE ORBIT SPECTRUM WITH SOLAR PROTONS
                                                                       SOFTP367
 730 WRITE(6,704)(TYPLBL(K,ITYPE),K=1,3),IT,IO,INALE,EXPECT,(ENERGY(M, SOFTMORR
    $ITYPE).AIFLXS(N).DIFFLX(N).DIFSPC(N).SPNRG(M).F(N).N=1.20).
                                                                       SOFTP369
                                                                       SOFTP370
    $(ENERGY(N.ITYPE),AIFLXS(N).DIFFLX(N).DIFSPC(N).N=21.30)
  704 FORMAT("+",41X,16("*"),3X,3A4,2X,16("*")/" ",41X,49("*")///T93,
                                                                       SOFTP371
    $!**** SOLAR PROTOMS ****!//T93, FOR TAU=!, 12, !, C=!, 12,!: MALE=!.
                                                                       SPETP372
     $I1/19X,15('*'), ' COMPOSITE ORBIT SPECTRUM ',15('*'),18X, 'WITH GEOWSOFIP373
    $AG SHIELDING'/T94, '(EXPOSE FACTOR='.F4.2,')'//19X.'ENERGY
                                                                   AVERSOFT P374
                               AVERAGED DIFF-1, 20X, 1 EMERGY
                DIFFERENCE
                                                                 TOTAL SOFIP375
    SAGED
                                                    REMITTAL FLUX!, 22X, SOFTP376
    $/19X, LEVELS
                    INTEGRAL FLUX INTEGRAL FLUX
                                          #/CM**2/SEC #/CM**2/SEC/DE
     $!LEVELS
                  FLUENCE'/19X,'>(MEV)
                                                                       SOFTH377
     $ #/CM**2/SEC/KEV!,20X,!>(MEV)
                                        #/CM**2!//20(T20,0PG9.4,T25,!
                                                                       SOFTP378
          *,1PE9.3.6X,1PE9.3.7X.1PE9.3,24X,0PF4.0.7X,1PF9.3/).10(T20.
                                                                       SOF 19379
                                                                       SOFTP380
    $0PG9.4.T25.1
                        ',1PE9.3.6X.1PE9.3.7X.1PE9.3/))
                                                                       SOFTP381
  750 CONTINUE
C *** PEAK AND TOTAL FLUXES PER PERIOD
                                                                       SOFTP383
     WRITE(6.2) MODEL, MODEL, BLTIME. NAME, INCL. IPRG, IAPG, ITAPE, PERIOD.
                                                                       SOF I P384
                                                                       SOFTP385
     WRITE(6,801)(TYPLBL(K.ITYPE),K=1.3),EMERGY(MRGYLV.ITYPE).
                                                                       SOFTP386
     5(N, (PKVALU(N, K), K=1,8), N=1, NRBITO)
                                                                       SOFIP387
                             !+!,T35,24(!*!),3X,3A4,2X,27(!*!)/! !,T35, SOFIP388
  801 FORMAT(
     $!** TABLE OF PEAK AND TOTAL FLUXES PER PERIOD : FMERGY >!.G9.2.T9750FIP389
          *MEV ***/* '.T35.68(***)//*0*.13X.*PERIOD
                                                      PEAK FLUX
                                                                     POSOFIP390
     5.
                                                  FIELD(B)
                                                              LIME(L) SOFIP391
     $SITION AT WHICH ENCOUNTERED
                                    ORBIT TIME
       TOTAL FLUX ! / ! . 13X , ! NUMBER
                                      ENCOUNTERED
                                                     LONGITUDE LATITUDSOFIP392
                                     * 1,23X, 1#/CM**2/SEC 1,2(5X, 1(DEG) 1SOFIP393
     $E ALTITUDE',41X,'PER ORBIT'/
     $),6X,'(KM)',7X,'(HOURS)',6X,'(GAUSS)
                                              (E.R.)
                                                         素/CM××2/ORBITISOFTP394
     $//(* *,14X,14,1PE14.3,0PF13.3,F10.2,F12.2,F13.5,F12.5,F10.2,1PF15.SOF1P395
                                                                       50FTP396
     53))
C *** ************* BLOCK 6: PROGRAM TERMINATION ******************************
                                                                       SOFIP398
  900 CONTINUE
                                                                        50FIP399
      GO TO 10
                                                                        SOFIP400
  999 STOP
      END
                                                                        SOFIP401
```

```
C *** *********** DIFFERENTIAL SPECTRUM SUBROUTINE ***********************DFSPC002
C *** CALCULATES FIRST DERIVATIVES OF INPUT SPECTRUM DEFINED BY FF VS XXDFSPC004
              XX - 30 INTEGRAL THRESHOLD ENERGIES. IN MEV
                                                               (R*4)DFSPC006
 *** INPHT:
C.
              FF - ALOG OF THE INTEGRAL FLUXES FOR THE 30 ENERGY (R*4)DFSPC008
C
 ***
                   LEVELS. IN PARTICLES/CM**2/SEC
                                                                    DESPC010
C.
 שלב שלב שלב
              DD - DIFFERENTIAL FLUXES OBTAINED FROM THE INTEGRAL (R*4)DFSPC012
C *** OUTPUT:
                   FLUXES. IN PARTICLES/CM**2/SEC/KEV
                                                                     DESPC014
 非非非
C.
 C *** THIS IS A MODIFIED VERSION OF A PROGRAM (DCS1EU) OBTAINED FROM
                                                                    DESPC018
C *** IMSL LIBRARY 1: AUTHOR/IMPLEMENTOR - C.L.SMITH
                                                                    DFSPC020
SUBROUTINE DSPCTR(FF.XX.DD)
                                                                    DFSPC024
      IMPLICIT REAL*8(A-H.O-Z)
                                                                     DESPC026
     REAL*4 DD.FF.XX
                                                                     DESPC028
     DIMENSION F(30),X(30),D(30),H(500),FF(30),XX(30),DD(30)
                                                                     DESPC030
     DATA EPSLN. OMEGA/1.D-6.1.0717968D0/
                                                                    DESPC032
                                                                     DFSPC034
C *** DATA INITIALIZATION
                                                                    DFSPC036
     M=()
     DO 5 L=1.30
                                                                     DESPC038
                                                                    DESPC040
    5 DD(L)=0.0
C *** DETERMINE SIZE OF ARRAY: OBTAIN M & K INDICES
                                                                     DFSPC042
       M = # OF NONZERO FLUXES - 1: K = # OF NONZERO FLUXES
                                                                     DFSPC044
      D0 10 K=1.30
                                                                     DESPC046
     IF(FF(K).E0.0.)
                         GO TO 15
                                                                    DESPC048
                                                                     DESPC050
     F(K) = FF(K) + ALOG(1000a)
                                                                     DESPC052
     X(K) = XX(K) \times 1000.00
                                                                     DFSPC054
   10 D(K)=X(K)
                                                                     DESPC056
   15 K=M+1
                                                                     DESPC058
     IF(K.LT.10) GO TO 170
                                                                     DFSPC060
C *** SMOOTHING INTEGRAL FLUX
                                                                     DESPC062
     CALL SMOOTH(X.F.M)
                                                                     DESPC064
 *** CALCULATE SECOND DERIVATIVES USING CENTRAL DIFFERENCES
                                                                     DFSPC066
                                                                     DESPC068
     DO 30 I=1.M
        H(I)=X(I+1)-X(I)
                                                                     DESPC070
        H(K + I) = (F(I+1)-F(I))/H(I)
   30
                                                                     DFSPC072
      DO 40
            I = 2 \cdot M
                                                                     DFSPC074
        H(2*X+I)=H(I-1)+H(I)
                                                                     DESPC076
        H(3*K+I) = .5*H(I-1)/H (2*K+I)
                                                                     DFSPC078
                                                                     DESPC080
        H(4*K+I)=(H(K+I)-H(K+I-1))/H(2*K+I)
                                                                     DFSPC082
        H(5*K+I)=H(4*K+I)+H(4*K+I)
                                                                     DFSPC084
        H(6*K+I)=H(5*K+I)+H(4*K+I)
      H(5*K+1)=0.
                                                                     DESPC086
```

```
H(6*K)=0.
                                                                            DFSPC088
C *** BEGIN ITERATION ON SECOND DERIVATIVES
                                                                            DFSPC090
      KCOUNT=0
                                                                            DFSPC092
   50 ETA=0.
                                                                            DFSPC094
                                                                            DFSPC096
      KCOUNT=KCOUNT+1
      DO 70 = 1=2.4
                                                                            DFSPC098
         W=(H(6*K+I)-H(3*K+I)*H(5*K+I-1)-(.5-H(3*K+I))*H(5*K+I+1)-H(5*K+DFSPC100
                                                                            DFSPC102
         I)*HMEGA)
         IF (DABS(W).LE.ETA) GO TO 60 .
                                                                            DFSPC104
         ETA=DABS(W)
                                                                            DFSPC106
         H(5*K+I)=H(5*K+I)+W
   60
                                                                            DFSPC108
   70 CONTINUE
                                                                            DFSPC110
      IF(KCOUNT.GT.5*K)GO TO 170
                                                                            DESPC112
      IF (ETA.GE.EPSLN) GO TO 50
                                                                            DFSPC114
C *** CONVERGENCE OBTAINED
                                                                            DFSPC116
      DO 80 I=1.4M
                                                                            DESPC118
         H(7*K+I)=(H(5*K+1+I)-H(5*K+I))/H(I)
   80
                                                                            DFSPC120
      DO 140 J=1.K
                                                                            DFSPC122
                                                                            DFSPC124
         IF (D(J).E0.X(1))GO TO 130
                                                                            DESPC126
         IF (D(J)-X(K)) 100,110,110
                                                                            DFSPC128
   90
         IF (D(J)-X(I)) 120.130.100
                                                                            DESPC130
  100
         I = I + 1
                                                                            DFSPC132
         GO TO 90
                                                                            DFSPC134
  110
         I = K
                                                                            DFSPC136
         J = [-]
                                                                            DFSPC138
  120
C *** COMPUTE D(J)
                                                                            DESPC140
  130
         HT1=D(J)-X(I)
                                                                            DFSPC142
         HT2=D(J)-X(I+1)
                                                                            DFSPC144
         DKUD=HII*HIS
                                                                            DFSPC146
         H(8*K+J)=H(5*K+I)+HT[*H(7*K+I)
                                                                            DFSPC148
         DELSOS = (H(5*K+I)+H(5*K+I+I)+H(8*K+J))/6.
                                                                            DFSPC150
  140
         D(J) = -(H(K + I) + (HT1 + HT2) * DELSOS + PROD*H(7*K + I) * . 1666667)
                                                                            DFSPC152
 *** SMOOTHING DIFFERENTIAL FLUX
                                                                            DFSPC154
      CALL SMOOTH(X.D.M)
                                                                            DESPC156
      DO 160 I=1.K
                                                                            DESPC158
      F(I)=2.71828182800**(F(I)-ALOG(1000.))
                                                                            DFSPC160
  160 DD(I)
                 =D(I)*F(I)
                                                                            DFSPC162
  170 RETURN
                                                                            DFSPC164
      END
                                                                            DFSPC166
C
                                                                            DESPC168
 *** SMOOTH DATA BY 3-POINT AVERAGING OVER EQUAL INTERVALS
                                                                            DFSPC170
      SUBROUTINE SMOOTH(X.F.M)
                                                                            DFSPC172
      IMPLICIT REAL*8(A-H•0-Z)
                                                                            DFSPC174
                                                                            DFSPC176
      DIMENSION X(30),F(30)
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```
FINTER(X1, X2, X3, Y1, Y2, Y3, XIN) = Y1*(XIN-X2)*(XIN-X3)/
                                                                           DESPU178
     s((X1-X2)*(X1-X3)) + Y2*(XIN-X1)*(XIN-X3)/((X2-X1)*(X2-X3))
                                                                           DESPUIRO
                         + Y3*(XIN-X1)*(XIM-X2)/((X3-X1)*(X3-X2))
                                                                           DFSPC182
C
                                                                           DFSPC184
      FI = F(1)
                                                                           DESPUIR6
      DO 20 I=2.M
                                                                           DESPUIRA
        SIZE1 = X(I) - X(I-1)
                                                                           DESPC190
        SIZE2 = X(I+1) - X(I)
                                                                           0FSPC192
C *** CHECK FOR EQUAL STEPSIZES
                                                                           DESPC194
        IF(DABS(SIZE1-SIZE2).LT.0.001) GO TO 200
                                                                           DESPU196
        IF(SIZE2.GT.SIZE1) GO TO 210
                                                                           DESPC198
C *** STEPSIZE DECREASES - FIT CURVE AND INTERPOLATE BACKWARD
                                                                           UFSPC200
        F2 = F(I+1)
                                                                           DESPC202
        XINTER = X(I) - SIZE2
                                                                           DESPUZO4
        F1 = FINTER(X(I-1), X(I), X(I+1), FI, F(I), F2, XINTER)
                                                                           DESPC206
        GO TO 300
                                                                           DESP0208
C *** STEPSIZE INCREASES ~ FIT CURVE AND INTERPOLATE FORWARD
                                                                           DESPC210
  210
        F1 = FI
                                                                           DFSPC212
        XINTER = X(I) + SIZE1
                                                                           OFSPC214
        F2 = FINTER(X(I-1),X(I),X(I+1),F1,F(I),F(I+1),XINTER)
                                                                           DESPU216
        GO TO 300
                                                                           DESPC218
C *** STEPSIZES ARE EQUAL - AVERAGE OVER EXISTING VALUES
                                                                           DESPC220
  200
        F1 = FI
                                                                           DFSPC222
        F2 = F(I+1)
                                                                           DFSPC224
C
                                                                           DFSPC226
 *** PERFORM AVERAGING
                                                                           DFSPC228
  300
        FNEW = (F1+2.0*F(I)+F2)/4.
                                                                           DESPU230
        FI = F(I)
                                                                           DESPU232
        F(I) = FNEW
                                                                           DESPU234
   20 CONTINUE
                                                                           DESPC236
      RETURN
                                                                           DESPC238
      END
                                                                           DESPC240
```

```
SUBROUTINE SOLPRO(TAU.IO.F.INALE)
                                                                        SOLPRO10
     MODIFIED 9/77 TO RETURN INALE(# OF AL EVENTS) TO CALLING PROGRAM
                                                                         SOLPRO20
 ***
      INTERPLANETARY SOLAR PROTON FLUX AT 1 AU (FROM E>10 TO E>200 MEV
                                                                        SOLPRO30
C
      FOR ANOMALOUSLY LARGE (AL) EVENTS AND FROM E>10 TO E>100 MEV FOR
                                                                        SOLPR040
 ***
      ORDINARY (OR) EVENTS)
C
                                                                        SOLPRO50
      SINGLE PRECISION DECK IN STANDARD FORTRAN IV FOR IBM 360 MACHINES SOLPRO60
C
 ***
 ***
C
      (EBCDIC, 029 PUNCH) OR OTHER COMPATIBLE SYSTEMS.
                                                                        SOLPR070
C
 *** PROGRAM DESIGNED AND TESTED BY E.G. STASSINOPOULOS, CODE 601.
                                                                         SOLPRO80
 *** NASA GODDARD SPACE FLIGHT CENTER, GREENBELT, MARYLAND 20771 .
                                                                         SOLPRO90
 ****************
                                                                        SOLPR100
C.
        INPUT: TAU
                       MISSION DURATION IN MONTHS (REAL*4)
                                                                        SOLPR110
C
               IO
                       CONFIDENCE LEVEL THAT CALCULATED FLUENCE F(N)
                                                                         SOLPR120
C
 ***
                       WILL NOT BE EXCEEDED (INTEGER*4)
                                                                         SOLPR130
                                                                         SOLPR140
C
 **** BUTPUT: F(N)
                       SPECTRUM OF INTEGRAL SOLAR PROTON FLUENCE FOR
C
 ***
                       ENERGIES E>10*N (1=<N=<20) FOR AL EVENTS
                                                                         SOLPR150
C ****
                       ENERGIES E>10*N (1=<N=<10) FOR OR EVENTS
                                                                         SOLPR160
C ****
               INALE
                       # OF AL EVENTS FOR GIVEN TAU AND O
                                                                         SOLPR170
      REAL NALE, NALECF (7,20)/-.1571,.2707,-.1269E-1,.4428E-3,-.8185F-5,
                                                                        SOLPR180
     5.7754E-7,-.2939E-9,-.1870,.1951,-.6559E-2,.1990E-3,-.3618E-5,
                                                                         SOLPR190
     $.3740E-7,-.1599E-9,-.2007,.1497,-.3179E-2,.5730E-4,-.4664E-6,
                                                                         SOLPR200
     $.1764E-8,0.,-.1882,.1228,-.1936E-2,.2660E-4,-.1022E-6,2*0.,
                                                                         SOLPR210
     $-.2214..1149,-.1871E-2,.2695E-4,-.1116E-6,2*0..-.2470,.1062,
                                                                         SOLPR220
     $-.1658E-2,.2367E-4,-.9465E-7,2*0.,-.2509,.8710E-1,-.8300E-3,
                                                                         SOLPR230
     $.8438E-5,3*0.,-.2923..8932E-1,-.1023E-2..1029E-4.3*0.,-.3222,
                                                                         SOLPR240
     $.8648E-1,-.9992E-3,.9935E-5,3*0.,-.3518,.8417E-1,-.1000E-2,
                                                                         SOLPR250
     $.9956E-5,3*0.,-.3698,.7951E-1,-.8983E-3,.8940E-5,3*0.,-.2771,
                                                                         SOLPR260
     $.5473E-1,-.1543E-4,4*0., -.2818,.5072E-1,.2511E-4,4*0.,-.2845,
                                                                         SOLPR270
     $.4717E-1,.5664E-4,4*0.,-.2947,.4405E-1..8507E-4,4*0.,-.2923,
                                                                         SOLPR280
     $.4111E-1,.1106E-3,4*0.,-.2981,.3853E-1,.1312E-3,4*0.,-.3002,
                                                                         SOLPR290
     $.3585E-1,.1529E-3,4*0.,-.3001,.3312E-1,.1781E-3,4*0.,-.3141,
                                                                         SOLPR300
     $.3248E-1..1654E-3.4*0./.F(20).G(20)
                                                                         SOLPR310
      REAL ORFLXC(5,9)/.154047E3,-.522258E4,.714275E5,-.432747E6,.955315SOLPR320
     $E6,.198004E3,-.448788E4,.438148E5,-.196046E6,.32552E6,.529120F3,
                                                                         SOLPR330
     $-.122227E5,.112869E6,-.465084E6,.710572E6,.121141E4,-.266412E5,
                                                                         SOLPR340
     $.226778E6,~.85728E6,.120444E7,.452062E4,-.103248E6,.896085E6,
                                                                         SOLPR350
     $-.346028E7,.499852E7,.272028E4,-.499088E5,.35305E6,-.111929E7,
                                                                         SOLPR360
     $.133386E7,.275597E4,-.469718E5,.314729E6,-.960383E6,.11165F7,
                                                                         SOLPR370
     $.570997E4,-.799689E5,.381074E6,-.610714E6,0.,.101E3,4*0./
                                                                         SOLPR380
      INTEGER INDEX(20)/2*7,6,3*5,5*4,9*3/
                                                                         SOLPR390
    1 FORMAT( TAU= 1, F4.0, 1 IQ= 1, I3, 3X, 1PARAMETER(S) EXCEED PROGRAM LIMISOLPR400
                                                                         SOLPR410
    2 FORMAT(2X, FOR THE COMBINATION OF TAU AND IQ GIVEN, NO SIGNIFICANTSOLPR420
```

```
$ SOLAR PROTON FLUXES ARE TO BE EXPECTED. TAU=',F6.2.' IO=',I2)
                                                                           SOLPR430
     IF(TAU.GT.72..OR.IO.LT.80)GD TO 500
                                                                           SOLPR440
      IP=100-I0
                                                                           SOLPR450
                                                                           SOLPR460
      M=INDEX(IP)
                                                                           SOLPR470
      NALF=0.
     DO 300 J=1.M
                                                                           SOLPR480
  300 NALE=NALE+NALECF(J.IP)*TAU**(J-1)
                                                                           SOLPR490
                                                                           SOLPR500
      INALE=NALE+1.0001
      IF(INALE.GT.O) GO TO 400
                                                                           SOLPR510
C *** CALCULATIONS FOR OR-EVENT CONDITIONS
                                                                           SOLPR520
                                                                           SOLPR530
                                                                           SOLPR540
      IF(IT.EO.1.AND.IP.GT.16) GO TO 700
      P=FLOAT(IP)/100.
                                                                           SOLPR550
                                                                           SOLPR560
      OF=0.
                                                                           SOLPR570
      DO 100 J=1.5
  100 OF=OF+ORFLXC(J.IT)* P**(J-1)*1.E7
                                                                           SOLPR580
                                                                           SOLPR590
      E = 10.
                                                                           SOLPR600
      DO 200 N=1,10
    G(N) = EXP(.0158*(30.-E))
                                                                           SOLPR610
                                                                           SOLPR620
     F(N)=0F*G(N)
                                                                           SOLPR630
  200 E=E+10.
                                                                           SOLPR640
      GO TO 800
                                                                           SOLPR650
C *** CALCULATIONS FOR AL-EVENT CONDITIONS
                                                                           SOLPR660
  400 E=10.
                                                                           SOLPR670
      DO 600 N=1,20
                                                                           SOLPR680 -
      F(N)=7.9E9*EXP((30.-E)/26.5)*INALE
                                                                           SOLPR690
  600 E=E+10.
      GO TO 800
                                                                           SOLPR700
                                                                           SOLPR710
  700 WRITE(6,2) TAU, IQ
     . GO TO 800
                                                                           SOLPR720
  500 WRITE (6,1) TAU, 10
                                                                           SOLPR730
                                                                           SOLPR740
  800 RETURN
                                                                           SOLPR750
      END
```

```
NAME = TEST 90/2000
INCL = 90
IPRG = 2000
IAPG = 2000
ITAPE = 5116
MODEL = 5
PERIOD = 2.119969
BLTIME = 1974.10
NRGLEV = 4
NTABLS = 3
CUTOFF = 23.99
ISKIP = 1
KPRINT = 1
```

Parameter Output

		赤冰水冰冰	PROT	ONS	(E> 5.00	MEV)	***	**	
LONG.	L AT .		ELD B-	LINE	DRBIT TIME	POSITION FLUX	AL	TIME-INTEG	ORBITAL FLUX(SUM)
(DEG)	(DEG)	(KM) (GA	บีรร)	(E.R.)	(HRS)	#/CM**2/5	EC		
-99.73	0.02		14110	1.36	0.0			0 0065 06	2.806E 06
-100.23	5.70		15100	1 - 42	0.03333	2.339E 1.692E	04	2.806E 06 2.031E 06	4.837E 06
-100.73	11.37		16342	1.51	0.06667	1.011E	04	1.213E 06	6.050E 06
-101-23	17.05		17749 19234	1.65	0.13333	4.953E	03	5.944E 05	6.644E 06
-101-73	22.72		20714	2.12	0.16667	3.589E	õã	4.307E 05	7.075E 06
-102.24 -102.74	28.39 34.06		22114	2.51	0.20000	9.497E	ŏž	1.140E 05	7.189E 06
-103.24	39.73		23371	3.09	0.23333	5.2655	01	6.318E 03	7.195E 06
-103.74	45.40	2002.8 0.	24437	3.96	0.26667	0.0		0.0	7.195E 06
-104-24	51.06		25282	5.36	0.30000	0.0		0.0	7.195E 06 7.195E 06
-104.74	56.73		25896	7.78	0.33333 0.36667	0.0		0.0	7.195E 06
-105-24	62.39		26294	12.43	0.40000	0.0		0.0	7.195E 06
-105.74 -106.25	68.05 73.71	2008.5 -1. 2009.4 -1.	00000	-1.00	0.43333	0.0		0.0	7.195E 06
-106.75	79.37	2010.0 -1.	00000	-i.00	0.46667	0.0		0.0	7.195E 06
-107.24	85.03		00000		0.50000	0.0		0.0	7.195E 06
72.19	89.31	2010.1 -1.	00000	-1.00	0.53333	0.0		0.0	7.195E 06
71.74	83.65		00000		0.56567	0.0		0.0	7.195E 06 7.195E 06
71 • 24 70 • 74	77.99	2008.8 0.	26230		0.60000	0.0 0.0		0.0	7.195E 06
70.74	72 - 33	2007.6 0.	25992 25619	7.58 5.25	0.63333 0.66667	0.0		0.0	7.195E 06
70.24 69.74	66.67 61.00	2004.5 0.	25076	3.87	0.70000	0.0		0.0	7.195E 06
69.24	55.34	2002.6	24343	3.01	0.73333	8.072E	01	9.686E 03	7.205E 06
68.74	49.67	2000.6 0.	23417	2.43	0.76667	7.752E	02	9.303E 04	7.298E 06
68.24	44.00	1998.6 0.	22314	2 • C4	0.80000	1.557E	03	1.868E 05	7.485E 06
67.74	38.32		21069	1.76	0.83333	1.659E	03 03	1.990E 05 4.930E 05	7.684E 06 8.177E 06
67.23 66.73	32.65		19741	1.57	0.86667 0.90000	4.108E 6.102E	03	7.322E 05	8.909E 06
66.73	26.97		18415	1.34	0.93333	8.266E	ŏΞ	9.9195 05	9.901E 06
66.23 65.73	21.29 15.61		16230	1.29	0.96667	1.031E	04	1.237E 06	1.114E 07
65.23	9.93		15608	1.26	1.00000	1.155E	04	1.386E 06	1.252E 07
64.73	4.25	1988.9 0.	15392	1.27	1.03333	1.350E	04	1.620E 06	1.414E 07
64 • 23	-1 -44		15554	1.31	1.06667	1 • 73 0E	04	2.076E 06 1.816E 06	1.622E 07 1.804E 07
63.72	-7.12		16002	1.38	1.10000	1.513E 1.491E	04 04	1.789E 06	1.983E 07
63.22	-12.80		16619	1.49	1.16667	1.205E	04	1.446E 06	2.127E 07
62.72 62.22	-18.48 -24.16		18010	1.87	1.20000	8.208E	03	9.850E 05	2.226E 07
61.72	-29.84		18701	2.17	1.23333	7.568E	03	9.081E 05	2.316E 07
61.22	-35.52		19380	2.57	1.26667	1.777E	60	2.133E 05	2.338E 07
60.72	-41.19	1997.6 0	20057	3.14	1.30000	7.793E	01	9.352E 03	2.339E 07 2.339E 07
60.22	-46.86		20739	3.94	1.33333	0.0		0.0	2.339E 07
59.71	-52.53		21427	5.10 6.87	1.36666	0.0		0.0	2.339E 07
58.71	-58.20 -63.86	2005.4 0	22789	9.61	1.43333	0.0		0.0	2.339E 07
58 21	-69.53	2007.0 0		13.83	1.46667	0.0		0.0	2.339E 07
57.71	-75.19	2008.3 -1	00000		1.50000	0.0		0.0	2.339E 07
57.21	-80.85		.00000		1.53333	0.0		0.0	2.339E 07 2.339E 07
56 • 71	-86.51		00000	-1.00	1 • 56667	0.0		0.0	2.339E 07
-123.80	-87.83			-1.00 -1.00	1.60000	0.0		0.0	2.339E 07
-124.30 -124.80	-82.17 -76.51	2010.2 -1.	24785	8.25	1.66667	0.0		0.0	2.339E 07
-125.30	-70.85	2009.0 0	24372	5.93	1.70000	0.0		0.0	2.339E 07
-125.80	-65.19	2007.9 0.	23761	4.45	1.73333	0.0		0.0	2.339E 07 2.339E 07
-126.30	-59.53	2006.6 0.	22970	3.48	1.76667	5 • 61 9E	00	6.743E 02 3.981E 04	2.339E 07 2.343E 07
-126.80	-53.87		22024	2 • 83	1.80000	3.318E 2.961E	03	3.553E 05	2.378E 07
-127.31	-48-20		.20956 .19802	2.37	1.86666	5.884E	03	7-060E 05	2.449E 07
-127.81 -128.31	-42.53 -36.87		18603	1.80	1.90000	6.749E	ŏ϶	8.099E 05	2.530E 07
-128.81	-31.20		17411	1.62	1.93333	1.168E	04	1.401E 06	2.670E 07
-129.31	-25.52	1997.2 0.	16288	1.50	1.96667	1.700E	04	2.040E 06	2.874E 07
-129.81	-19.85		15309	1 . 41	2.00000	2 • 1 4 3 E	04 04	2.572E 06 3.121E 06	3.131E 07 3.443E 07
-130.31	-14.18	1995.0 0	1 4558	1, . 35	2.03333	2.601E	04	3.121E 00	34435 07

```
2.343E 03
9.136E 04
8.012E 05
 -84.17 -65.24
                       2008.1 0.20507 3.42
                                                       22.89999
                                                                      1.952E 01
                                                                                                       8.400E 08
 -84.67 -59.58
-85.17 -53.91
-85.08 -48.25
                                                      22.93330
22.96666
22.99998
23.03331
                                                                      7.613E 02
6.676E 03
                       2006.9
                                  0.19271
                                              2.76
                                                                                                       8.401E 08
                       2005.4
                                  0.18030
                                              2.31
                                                                                                       8.409E 08
                                                                      1.580E 04
                                                                                      1.896E 06
2.502E 06
                                                                                                       8.428E 08
8.453E 08
                       2003.8
                                 0.16828 2.00
 -86.18 -42.58
                       2002.2
                                  0.15704
                                              1.78
                                                                      2.085E 04
                                                                      3.203E 04
 -86.68 -36.91
-87.18 -31.25
                                                       23.06667
                                                                                       3.844E 06
                                                                                                       8.4915 08
                                 0.14696
                                              1.62
                       2000.5
                                              1.51
                                                       23.09999
                                                                      4.250E 04
                                                                                      5.100E '06
                                                                                                       8.542E 08
                       1999.0
 -87.68 -25.57
-88.18 -19.90
                       1997.5
                                  0.13194
                                              1.43
                                                       23.13332
                                                                      4.992E 04
                                                                                      5.991E 06
                                                                                                       8.602E 08
                       1996.3 0.12800
                                              1.38
                                                                      5.732E 04
                                                                                      6.878E 06
                                                                                                       8.671E 08
                                                       23.16664
 -88.68 -14.23
-89.18 -8.55
-89.69 -2.88
                       1995.4
1994.7
                                  0.12716
                                             1.35
1.35
                                                       23.20000
23.23331
                                                                      5.855E 04
5.195E 04
                                                                                      7.026E 06
6.234E 06
                                                                                                       8.741E 08
                                                                                                       8.803E 08
8.851E 08
8.885E 08
                                 0.12983
                                              1.37
                                                                      3.948E 04
2.863E 04
2.068E 04
                                                                                      4.738E 06
                       1994.3
                                  0.13610
                                                       23.26666
                                 0.14567 1.42
0.15790 1.50
0.17196 1.62
                                                                                      3.436E 06
2.482E 06
1.526E 06
                       1994.3
1994.7
                                                       23.29999
 -90.19
             2.80
                                                                                                       8.910E 08
8.925E 08
 -90.69
             8.47
 -91.19 14.15
                                                       23.36664
                                                                      1.272E 04
                       1995.3
 -91.69
            19.82
                       1996.3
                                 0.18700
                                              1.80
                                                                      6.474E 03
                                                                                      7.769E 05
                                                                                                       8.933E 08
 -92.19
            25.49
                       1997.5
                                  0.20217
                                              2.05
                                                       23.43330
                                                                      4.860E 03
                                                                                      5.833E 05
                                                                                                       8.939E 08
                                                       23.46666
 -92.69
            31.16
                       1998.9
                                  0.21671 2.41
                                                                      2.435E 03
                                                                                       2.922E 05
                                                                                                       8.942E 08
                                                       23.49998
23.53331
23.56667
                                                                                                       8.942E 08
8.942E 08
8.942E 08
 -93.19
            36.83
                       2000.4
                                  0.22995
                                              2.92
                                                                      1.340E 02
                                                                                      1.608E 04
 -93.70
-94.20
                       2002.1
                                 0.24136 3.71
0.25058 4.94
           42.50
                                                                      0.0
                                                                                      0.0
                                                                                      0 - 0
 -94.70
                       2005.3 0.25745
                                              7.02
            53.83
                                                       23.59999
                                                                      0.0
                                                                                                       8.942E 08
                                                                                      0.0
 -95.20
            59.50
                       2006.8
                                  0.26205 10.93
                                                       23.63332
                                                                                                       8.942E 08
                                                                      0.0
                                                                                      0.0
 -95.70
            65.16
                       2008.0 0.26466 19.48
                                                       23.66664
                                                                                       0.0
                       2008.0 0.26466 19.48

2009.0 -1.00000 -1.00

2009.8 -1.00000 -1.00

2010.1 -1.00000 -1.00

2010.2 -1.00000 -1.00

2009.9 -1.00000 -1.00

2009.2 0.225379 15.41

2008.1 0.26251 9.18
 -96.20
            70.82
                                                       23.70000
                                                                      0.0
                                                                                      0.0
                                                                                                       8.942E 08
                                                       23.73331
23.76666
23.79999
 -96.70
            76 • 48
                                                                      0.0
                                                                                      0.0
                                                                                                       8.942E 08
8.942E 08
 -97.20
-97.70
           82.14
                                                                      0.0
                                                                                      0.0
                                                                                      0.0
                                                                                                       8.942E 08
  81 . 78
                                                       23.83331
                                                                                                       8.942E 08
                                                                      0.0
           86 4 54
                                                                                      0.0
  81.29
80.79
           80.88
75.22
                                                       23.86664
                                                                      0.0
                                                                                      0.0
                                                                                                       8.942E 08
                                                       23.89999
                                                                      0.0
                                                                                      0.0
                                                                                                       8.942E 08
                       2006.8 0.26016 6.12
2005.2 0.25625 4.40
   80.29 69.56
                                                       23.93330
                                                                      0.0
                                                                                                       8.942E 08
                                                                                      0.0
  79.78 63.90
                                                       23.96666
                                                                      0.0
                                                                                      0.0
                                                                                                       8.942E 08
***** PERCENT OF TOTAL LIFETIME SPENT INSIDE AND CUTSIDE TRAPPED PARTICLE RADIATION BELT ****
      INNER ZONE (1.0 <= L < 2.8) : 51.60 %
      OUTSIDE TRAPPING REGION (1.0 <= L < 1.1): 0.0 %
INSIDE TRAPPING REGION (1.1 <= L < 2.8): 51.60 %
OUTER ZONE (2.8 <= L <= 11.0): 26.84 %
EXTERNAL (L > 11.0): 21.56 %
                                                                                                                                                Percent Time Table
TOTAL ORBIT TIME IS : 24.00 HOURS
```

\*

## \*\*\*\*\*\*\*\*\* COMPCSITE ORBIT SPECTRUM \*\*\*\*\*\*\*\*\*\*

ENERGY	AVERAGED	DIFFERENCE	AVERAGED DIFFE-
LEVELS	INTEGRAL FLUX	INTEGRAL FLUX	RENTIAL FLUX
> (MEV)	#/CM**2/SEC	#/CM**2/SEC/DE	#/CM**2/SEC/KFV
2.000	1.646E 04 1.401E 04	2.454E 03 1.667E 03	0.0
4.000	1.234E 04	1.218E 03	0.0
5.000	1.112E 04	9.428E 02	
6.000	1.018E 04	1.615E 03	0 • 0
8.000	8.564E 03	1.247E 03	0 • 0
10.00	7.318E 03	1.642E 03	0 • 0
15.00	5.675E 03	1.203E 03	0.0
20.00	4.472E 03	4.420E 02	
25.00	4.030E 03	3.913E 02	0 • 0
30.00	3.639E 03	2.295E 02	0 • 0
35.00	3.409E 03	2.138E 02	0 • 0
40.00	3.195E 03	1.993E 02	0 • 0
45.00	2.996E 03	1.860E 02	0 • 0
50.00	2.810E 03	1.528E 02	0 • 0
55.00	2.657E 03	1.4415 02	0.0
60.00	2.513E 03	2.642E 02	
70.00	2.249E 03	2.355E 02	0 • 0
80.00	2.014E 03	2.100E 02	0 • 0
90.00	1.804E 03	1.874E 02	0 • 0
100.0	1.616E 03	3.818E 02	0 • 0
125.0	1.234E 03	2.901E 02	0 • 0
150.0	9.444E 02	2.209E 02	0 • 0
175.0	7.235E 02	1.685E 02	0.0
200.0	5.5495 02	2.143E 02	
250.0	3.407E 02	1.311E 02	0.0
300.0	2.096E 02	8.042E 01	0.0
350.0	1.292E 02	4.944E 01	0.0
400.0	7.973E 01	4.925E 01	0.0
500.0	3.047E 01	3.047E 01	

### \*\*\*\*\*\*\*\*\*\* CCMPOSITE ORBIT SPECTRUM \*\*\*\*\*\*\*\*\*\*\*

ENERGY LEVELS >(MEV)	AVERAGED INTEGRAL FLUX #/CM**2/SEC	DIFFERENCE INTEGRAL FLUX #/CM**2/SEC/DE	AVERAGED DIFFE- RENTIAL FLUX #/CM**2/SEC/KEV
1000 1000	7.454E 06 2.738E 06 1.217E 06 6.538E 05 3.576E 05 1.728E 05 1.728E 05 1.012E C5 1.012E C5 1.012E C4 1.334E 04 2.021E C4 1.334E C4 1.334E C4 1.334E C3 2.188E 03 1.185E C3 7.055E C2 2.868E 02 2.868E 02 2.868E 02 2.868E 02 2.868E 01 3.252E 01 3.583E 01	4.716E 06 1.521E 06 5.630E 05 2.962E 05 1.11E 05 7.425E 04 4.388E 04 2.718E 04 2.117E 04 1.677E 04 1.677E 04 1.677E 04 1.677E 04 2.627E 03 2.740E 03 3.930E 03 2.740E 03 3.937E 03 1.003E 03 2.749E 02 2.667E 02 1.484E 02 7.141E 01 1.669E 01	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
5.500 6.000 6.500	1.550E 00 2.509E-02 0.0	1.525E 00 2.509E-02 0.0	0.0 0.0 0.0 0.0
7.000	0.0	0.0	0.0

## \*\*\*\* SOLAR PROTONS \*\*\*\*

*****	******* COMPOS	ITE ORBIT SPECTE	JM *********	WITH GEOM	Q=90: NALE=1 AG SHIELDING ACTOR=0.34)	** EXPOSURE	INDEX: ENER	GY>5.000 MEV **
ENERGY LEVELS >(MEV)	AVERAGED INTEGRAL FLUX #/CM**2/SEC	DIFFERENCE INTEGRAL FLUX #/CM**2/SEC/DE	AVERAGED DIFF- RENTIAL FLUX */CM**2/SEC/KEV	ENERGY LEVELS > (MEV)	TOTAL FLUENCE #/CM**2	INTENSITY RANGES #/CM* *2/SEC	EXPOSURE DURATION (HOURS)	TOTAL # OF ACCUMULATED PARTICLES
2.000 3.000 4.000 5.000 6.000 10.00 20.000 25.00 25.00 30.00 40.00 40.00 50.00 50.00 50.00 100.	1.504E 04 1.291E 04 1.144E 04 1.145E 04 1.145E 03 6.768E 03 6.768E 03 4.136E 03 3.110E 03 3.110E 03 2.7727E 03 3.110E 03 3.110	2.134E 03 1.468E 03 1.089E 02 1.536E 03 1.5196E 03 1.5196E 03 1.113E 03 1.113E 03 1.113E 02 2.165E 02	2.24 2E 00 1.72 8E 00 1.72 8E 00 1.29 7E 00 1.29 7E 00 8.39 5E-01 4.68 9E-01 2.52 9E-01 1.47 10E-02 2.52 9E-02 2.52 5E-02 2.76 25E-02	10. 20. 40. 50. 60. 70. 80. 90. 110. 120. 140. 150. 160. 170. 180. 190.	5.741E 09 3.937E 09 2.699E 09 1.851E 09 1.2699E 09 8.701E 08 5.966E 08 4.091E 08 2.805E 08 1.319E 08 1.319E 08 9.042E 07 4.251E 07 1.999E 07 1.9799E 07 1.3796E 06 6.443E 06	ZERO FLUX 1 • E0 - 1 • E1 1 • E2 - 1 • E3 1 • E2 - 1 • E4 1 • E4 - 1 • E5 1 • E5 - 1 • E6 1 • E6 - 1 • E7 1 • E7 - OVER TOTAL	10.100 0.100 1.000 1.333 5.000 6.267 0.167 0.0 23.964	0.0 2.749E 03 1.686E 05 2.225E 06 8.745E 07 7.407E 08 6.368E 07 0.0 0.0 8.942E 08

## 

#### \*\*\*\* SCLAR PROTONS \*\*\*\*

****	****** CGMPOS	ITE ORBIT SPECTR	UM ***********	WITH GEOM	Q=90: NALE=1 AG SHIELDING ACTUR=0.34)	** EXPOSURE	INDEX: ENER	GY>.5000 MEV **
ENERGY LEVELS >(MEV)	AVERAGED INTEGRAL FLUX #/CM**2/SEC		AVERAGED DIFF- RENTIAL FLUX #/CM**2/SEC/KEV	ENERGY LEVELS >(MEV)	TGTAL FLUENCE #/CM**2	INTENSITY RANGES #/CW**2/SEC	EXPOSURE DURATION (HOURS)	TOTAL # OF ACCUMULATED PARTICLES
.1000 .2000 .3000 .4000 .5000 .7000 .9000 1.250 1.5750 2.0250 2.55	1.511E 07 7.076E 06 1.154E 06 1.154E 05 1.976E 05 1.9746E 05 1.9746E 05 1.0746E 04 1.0443E 04 1.0443E 04 1.0456E 04 1.0456E 04 1.0456E 04 1.0456E 04 1.0456E 04 1.0556E 04 1.0556E 04 1.0556E 04 1.0556E 04 1.0556E 04 1.0556E 03 1.055	8.096E 06 4.037E 06 1.821E 06 6.924E 05 1.672E 05 1.672E 05 1.672E 05 1.672E 04 2.455E 02 2.455E 03 3.395E 03 3.395E 03 3.395E 03 3.395E 02 2.455E 02	1.175E 05 5.685E 04 2.557E 04 9.787E 03 3.515E 03 1.461E 03 7.461E 02 4.435E 02 2.844E 02 1.869E 01 3.426E 01 2.2588E 01 3.426E 01 1.673E 01 1.791E 00 5.154E 00 1.8791E 00 1.8891E 00	10 · 20 · 30 · 40 · 50 · 60 · 70 · 80 · 90 · 100 · 120 · 120 · 150 · 160 · 170 · 180 · 190 · 200 ·	5.741E 09 3.937E 09 2.669E 09 1.851E 09 1.851E 09 8.701E 08 5.966E 08 4.091E 08 2.805E 08 1.319E 08 1.319E 08 9.042E 07 4.251E 07 2.9915E 07 1.9396E 07 1.9396E 06 6.443E 06	ZERO FLUX 1.E0-1.E1 1.E1-1.E2 1.E2-1.E3 1.E3-1.E4 1.E4-1.E5 1.E5-1.E6 1.E5-1.E7 1.E7-0VER TOTAL	£.333 0.033 0.200 0.333 1.733 3.267 9.367 0.00 0.0	0.0 2.171E 02 1.575F 04 5.981E 05 2.886E 07 5.272E 08 1.317E 10 2.619E 10 0.0 3.993E 10

# 

PERIOD NUMBER	PEAK FLUX ENCOUNTERED #/CM**2/SEC	PCSITION LONGITUDE (DEG)	AT WHICH EN	NCOUNTERED ALTITUDE (KM)	ORBIT TIME (HOURS)	FIELD(B)	LINE(L) (E.R.)	TOTAL FLUX PER ORBIT #/CM**2/ORBIT
1	3.253E 04	-131.316	-2.83	1993.99	2.10000	0.14041	1.31	4.552E 07
. 2	3.599F 04	31.637	-9.95	1989.39	3.23333	0.14089	1.46	6-160E 07
<u>3</u>	6.541E 04	-0.451	-12.79	1989.68	5.36666	0.12769	1.50	8.547E 07
4	1.059E 05	-33.040	-21.31	1991.28	7.53333	0.11669	1.50	1.200E 08
Ś	9.788E 04	-64.626	-18.46	1990.65	9.63333	0.11720	1.39	9.174E 07
6	4.973E 04	-96-212	-15.62	1990-13	11.73333	0.13084	1.35	5.599E 07
7	3.321E 04	-127.298	-7.08	1988.98	13.80000	0.13994	1.31	6.099E 07
Ŕ	5.778E 04	6.577	-11.38	1994.78	16.86664	0.13019	1.49	7.891E 07
ă	9.856E 04	-25.511	-8.54	1994.54	18.99998	0.11706	1.40	1.1872 08
1 Ó	1.099E 05	-56.596	-17.06	1995.76	21.06667	0.11493	1.40	1.089E 08
iĭ	5.855E 04	-88.683	-14.23	1995.36	23.20000	0.12716	1.35	6.306E 07

# 

PER IOD NUMBER	PEAK FLUX ENCOUNTERED #/CM**2/SEC	POSITION LONGITUDE (DEG)	AT WHICH EN LATITUDE (DEG)	COUNTERED ALT (TUDE (KM)	ORBIT TIME (HOURS)	FIELD(8) (GAUSS)	LINE(L) (E•R•)	TOTAL FLUX PER ORBIT #/CM**2/ORBIT
1	1.980E 06	-129.812	-19.85	1995.97	2,00000	0.15309	1.41	2.649E 09
ā	2.216E 06	31.637	-9.95	1989.39	3,23333	0.14089	1.46	3.260E 09
3	2.940E 06	0.051	-7.11	1989.01	5.33333	0.12639	1.42	3.779E 09
ã.	3.536E 06	-32.538	-15.63	1990.08	7.50000	0.11529	1.44	4.472E 09
Š	3.309E 06	-65.127	-24-14	1992.01	9.66667	0.11888	1.43	3.650E 09
6	2.405E 06	-97.215	-26.98	1992.32	11.80000	0.14082	1.45	2.971E 09
7	2.337E 06	38.162	-8.54	1994.46	14.76667	0.1430.6	1.43	3.259E 09
8	2.805E 06	6.075	-5.70	1994.27	16.89999	0.12839	1.41	3,710E 09
9	3.508E 06	-25.009	-14.22	1995.21	18,96666	C-11709	1.45	4.749E 09
10	3.504E 06	-56,094	-22.73	1996.85	21.03331	0.11561	1.44	4.193E 09
īi	2.730E 06	-87.680	-25.57	1997.54	23.13332	0.13194	1.43	2,986E 09



National Aeronautics and Space Administration

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